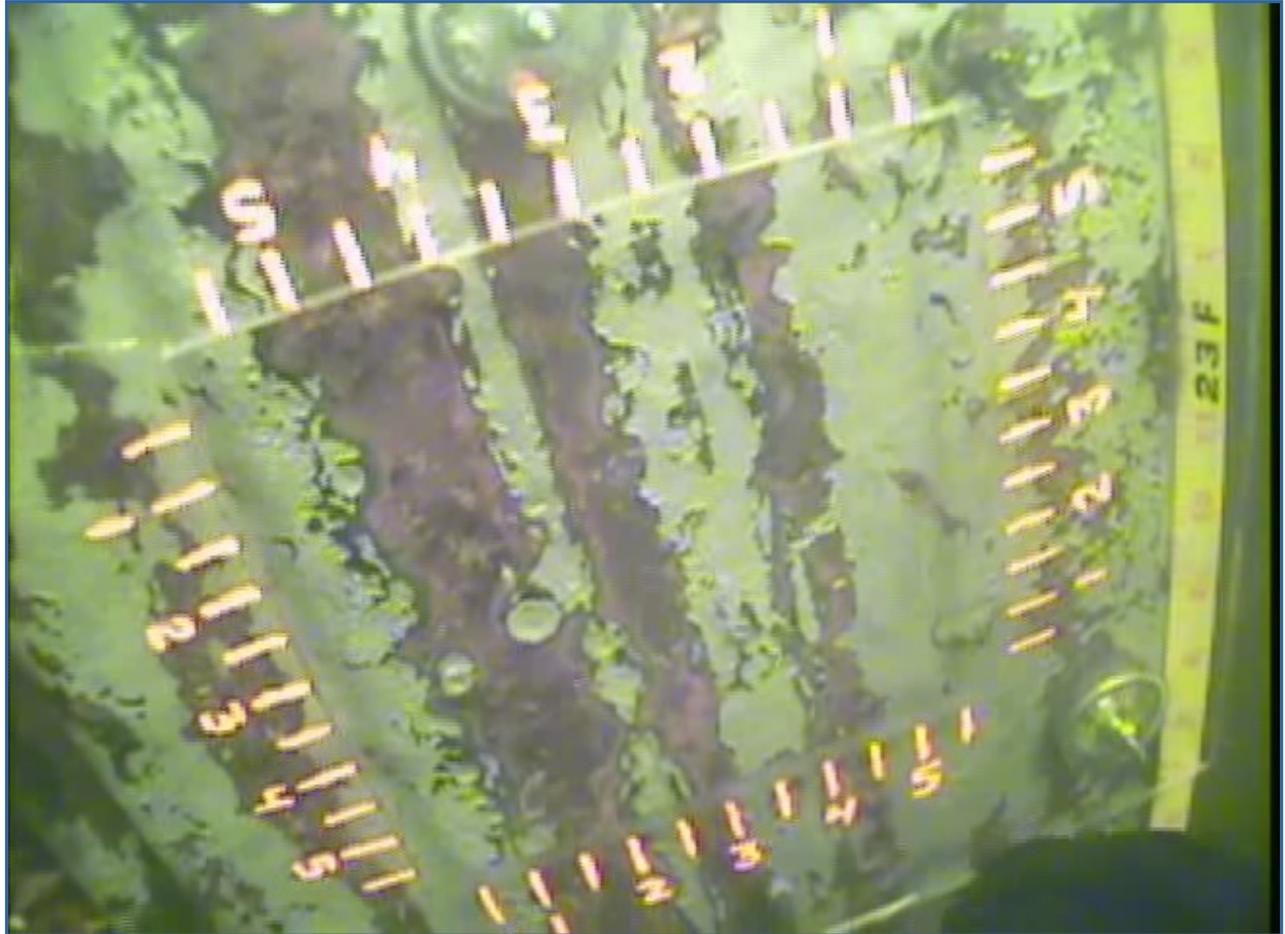


DSPA CORROSION INVESTIGATION REPORT



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DSPA CORROSION INVESTIGATION REPORT

AMI #061016 DATE: JULY to DECEMBER, 2006

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Project Description

The Accelerated Freshwater Corrosion Study in the Duluth / Superior Harbor was initiated in 2003 to further investigate the findings of preliminary accelerated corrosion data. In 2004, a panel of corrosion experts was brought together by the financial support by the Minnesota and Wisconsin Sea Grant programs, the University Of Minnesota Duluth (UMD) Natural Resources Research Institute the Army Corps of Engineers (ACOE) and the Duluth Seaway Port Authority (DSPA). The results from the corrosion expert panels two day workshop was published by the Army Corps of Engineers in the ERDC/CERL SR-05-3 publication dated March 2005. The panel of experts present made recommendations on future short and long term testing which would be necessary to narrow down the list of possible causes of accelerated corrosion and to determine the full extent of the process around the entire harbor. The recommendations for the short term included corrosion rate monitoring, water chemistry analysis, corrosion product and microbiologically induced corrosion (MIC) analysis, stray current testing and the critically needed condition assessments and structural characterization. Long term recommendations included condition based inspection strategy for repair / replacement management, ongoing monitoring, developing a standard replacement design using both coatings and cathodic protection (CP), and initiating a corrosion characterization survey of other great lakes port facilities.

Scope of Work

The scope of work included in this report was recommended by the expert panel as the short term recommendations for the corrosion study. Through funding from the Minnesota DNR, the Duluth Seaway Port Authority was able to contract with AMI Consulting engineers to complete the following investigations and data gathering on the non-federal structures:

- Non-Federal Structure Data Gathering
- Underwater visual and tactile inspection
- Non destructive testing
- Water Quality Measurements (Bulk water completed by ACOE)
- Corrosion rate measurements
- Biological Sampling (testing to be completed by UMD)
- Coupon tray engineering, design and installation
- Complete documentation

All data was to be collected and reported in a manner consistent with the needs of the study being undertaken by both the DSPA and the Army Corps of Engineers. Through meetings with the local corrosion committee members, the Duluth Superior harbor inspection points were located and chosen based on their proximity to one another throughout the harbor and based on the existence of adequate steel members to be inspected. The sample points extended from the Oliver Bridge in the St Louis River to the harbor entries on both the Superior and Duluth sides. All structures would require very precise timing and coordination because of the significant shipping activity in these areas and the abrupt change in weather affecting the sites.

AMI Consulting Engineers utilized our 22 foot Hewes Craft pilot house dive boat with a 200HP Honda motor and a surface supplied dive spread. The diver's surface supplied air was provided from a high pressure bank system to the diver's helmet. The primary helmet was a SL-27 with a band mask standby system. Bailout bottles were required for



all dives. The diver's visual inspections were documented utilizing an Outland color video camera and light. This system was connected to a computer system capable of collecting and backing up all video data collected. The non-destructive testing equipment utilized for the project was a Dakota Ultrasonics MX3 system with an underwater housing and transducer. The system was calibrated with a certified calibration step block, 4340 FE SN#06-1200, before every use to insure accuracy of the measurements. Standard dive and field data forms were generated and utilized to collect all the general field data and then transferred into the electronic forms.

AMI Consulting Engineers provided the following detailed scope of services as directed by Jim Sharrow of the DSPA:

The detailed scope of services finalized was as follows:

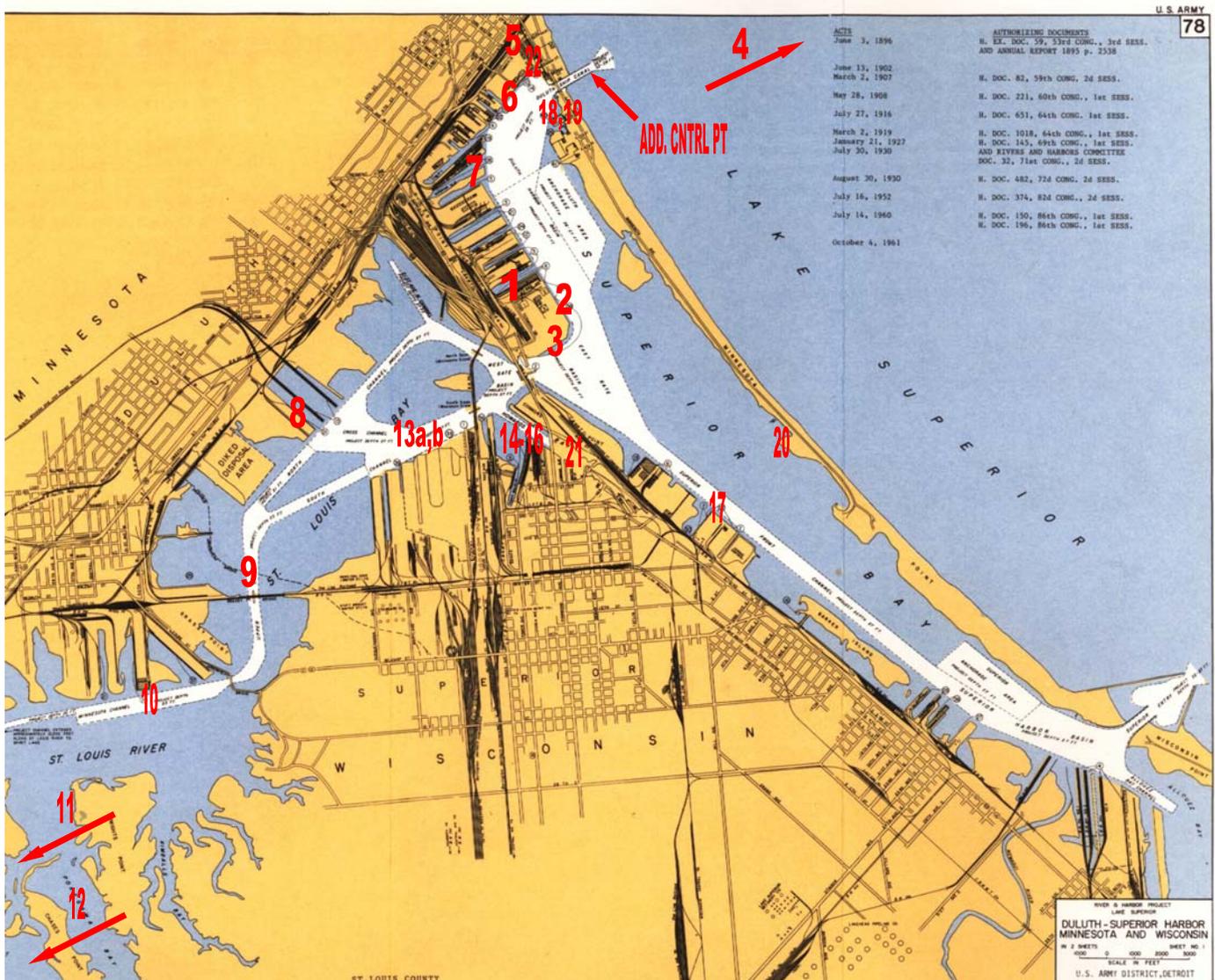
- Attend a meeting with the DSPA and other corrosion committee members to organize the investigation and set protocols for work at the selected investigation sites.
- Developed with the DSPA a permission form and release for work on private property selected. Acquired signed permission and submitted insurance certificates to each property owner.
- Prepared a dive plan policy and procedures, emergency action assessment and safety plan.
- Developed protocol to advise the local authorities and private owners on weekly and daily movement for security concerns.
- Prepare all pre/ post dive and field collection forms.
- Provided all dive equipment, cleaning equipment, digital video camera equipment, GPS and Non destructive testing equipment.
- Provide a three man dive team meeting all OSHA, Coast Guard and ADCI standards and regulations for commercial diving.
- Properly mark above the waterline a permanent reference mark to IGLD with a grinder and record GPS location data in Latitude/Longitude format.
- Perform specific underwater visual and tactile inspections on all approved non-federal structure locations. Inspections included all cleaning, NDT and corrosion measurements
- Documented conditions with digital video system.
- Recorded all marine growth notes, overall plate thickness measurements, 4 pit depth readings, 4 diameter readings and concentrations at two foot elevation to -10 feet IGLD and then five foot increments to the mud line. All measurements were taken within a 6"x6" relative area for comparison.
- Performed instantaneous water quality measurements utilizing the Quanta Hydro Lab.



- Assisted Dr. Randall Hicks at UMD in the collection of biological samples.
- Performed instantaneous Linear Polarization corrosion rate measurements.
- Designed, fabricated and installed coupon trays and coupons.

Field Data Collection

The collection of the underwater data and topside data was conducted between the dates of July 20th 2006 and November 29th, 2006. The project started with the inspections at the DSPA Berth 1 and ended with the final corrosion measurements at the Duluth entry. To provide proper time management and minimize down times, the water quality measurements and the underwater corrosion measurements were taken at the same time.





Site 1-DSPA Bulkhead Berth 1 - Duluth

The DSPA Berth 1 facility is operated by Lake Superior Warehousing and consisted of a steel sheet pile bulkhead with a metal cap. This facility sees moderate use for the receipt and shipping of general cargo in foreign and domestic trade, including heavy lift items and finished steel products. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD and below on the out pans and instantaneous water quality measurements. Nothing unusual was noted at the site.

Site 2- DSPA Bulkhead Berth 4 – Duluth

The DSPA Berth 4 facility is operated by the Murphy Oil USA company and consisted of a steel sheet pile bulkhead with a metal cap. This facility sees high use for the refueling of all types of vessels for both the foreign and domestic trade. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD and below on the out pans, instantaneous water quality measurements and instantaneous corrosion measurement. This site was fitted with a coupon tray with coupons for measurements in 2007. This site has seen a high amount of scour due to the activity level.

Site 3- DSPA Bulkhead Berth 6 – Duluth

The DSPA Berth 6 facility is operated by the DSPA and consisted of a steel sheet pile bulkhead with a metal cap. This facility sees low use for the receipt and shipping of general cargo in foreign and domestic trade, including heavy lift items. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. Nothing unusual was noted at the site.

Site 4- CN Dock 1 – Two Harbors

The CN Dock 1 is an iron ore pellet vessel loading dock which services both domestic and international shipping. The dock is located outside the Duluth Superior harbor in Agate bay off Lake Superior in Two Harbors, MN. There is a breakwater dividing the small safe harbor from the lake. The bulkhead consists of steel sheet piling with a concrete cap and has recently seen relatively low use. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. The corrosion was generally less concentrated than on the Duluth Superior Harbor structures and appeared to be in much larger connected masses when present. The dome shaped nodules were not present, but a similar thick orange mass was present over the corroded areas.

Site 5- Minnesota Slip Bulkhead - Duluth

The Minnesota Slip bulkhead is operated by the City of Duluth and consists of a steel sheet pile bulkhead with a metal cap. This facility only receives charter, museum and pleasure craft. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. A city storm sewer outlet was



present and flowing within 15 feet of the measurement site.

Site 6- DECC Bulkhead- Duluth

The DECC bulkhead is operated by the City of Duluth and consists of a steel sheet pile bulkhead with a metal cap. This facility receives charter, museum, cruise vessels and tour boat craft. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements.

Site 7- Cargill Bulkhead - Duluth

The Cargill bulkhead is owned and operated by Cargill Inc. The bulkhead consists of a steel sheet pile bulkhead with a metal cap. This facility only sees moderate use for the export shipping of general grains for foreign and domestic trade. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. The steel at this site was perforated.

Site 8- Hallett Dock 5 - Duluth

The Hallett 5 bulkhead is owned and operated by Hallett Dock Company. The bulkhead consists of a steel sheet pile bulkhead with a metal cap. This facility only sees moderate use for the import of general bulk materials. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans, instantaneous water quality measurements and instantaneous corrosion measurements. This site was fitted with a coupon tray with coupons for measurements in 2007.

Site 9- Mn/DOT Bong Bridge Cell – Duluth

The Bong Bridge protective cell is owned and maintained by the Minnesota DOT. The cell consists of flat steel sheet pile with a concrete cap. This cell only sees low activity for the protection of the bridge piers from ships that may accidentally lose control in the main shipping channel. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. The steel at this site was originally coated with some form of coal tar epoxy during erection which has retarded the corrosion.

Site 10- Hallett Dock 7

The Hallett 7 bulkhead is owned and operated by Hallett Dock Company. The bulkhead consists of wood Wakefield piling and a concrete cap. This facility only sees low use for the import of general bulk materials. The field data collection for this site included instantaneous water quality measurements and instantaneous corrosion measurements. This site was fitted with a coupon tray with coupons for measurements in 2007.

Site 11- Spirit Lake Marina Pipe Piles – Duluth

The Spirit Lake Marina is operated privately by Judy King. The docks are primarily timber support open wood piling. The area inspected was repaired with sections of steel



pipe allowing for the inspection of an additional steel structure this far up stream. This facility only receives charter and pleasure craft. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the bottom of the steel jackets and instantaneous water quality measurements. Tate & Lyle Chemical has a plant intake and power transformer structure located on the adjacent property only 50 feet from the measurements at Spirit Lake Marina.

Site 12- CN Oliver Bridge Pier – Oliver

The Oliver Bridge is owned and operated privately by the CN Railway. The Bridge is primarily constructed with concrete piers. Due to a scour problem around the western pier, steel sheet piling was added to prevent undermining of the bridge pier foundation. The channels on each side of the bridge piers only see pleasure craft. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans, instantaneous water quality measurements and instantaneous corrosion measurements. This site was fitted with a coupon tray with coupons for measurements in 2007. It was also noted during a private bridge inspection that the steel nosing for ice breaking purposes on the upstream side of the bridge piers had heavy pitting which is consistent with the findings on the sheet piling.

Sites 13a & b- Midwest Energy Resources Wharf – Superior

The Midwest Energy wharf is owned and operated by Midwest Energy. The wharf consists of an open steel H-pile bulkhead with a reinforced concrete deck. This facility sees very high usage for the export of coal. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans, instantaneous water quality measurements and instantaneous corrosion measurements. This site was fitted with a coupon tray with coupons for measurements in 2007.

Site 14- Cenex Harvest States East Bulkhead – Superior

The CHS East bulkhead is owned and operated by Cenex Harvest States. The bulkhead consists of a steel sheet pile bulkhead with a deep concrete cap (extending to 3 feet below IGLD) over 75% of the entire bulkhead. This facility only sees moderate use for the export of grain products. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from -3 feet IGLD to the mud line on the out pans and instantaneous water quality measurements. A storm water outlet is present at the inner end of the slip.

Site 15- Cenex Harvest States West Bulkhead – Superior

The CHS West bulkhead is owned and operated by Cenex Harvest States. The bulkhead consists of a steel sheet pile bulkhead with a concrete cap over the entire inner 550 feet of bulkhead. This bulkhead is scheduled for replacement due to perforations, soil loss and anchorage concerns. This inner end of the facility is only used to retain the soil under the dock structure which supports the grain bins next to the waterfront. These bins are used for the storage of different grain products which are exported. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. Nothing else unusual was noted at the site.



Site 16- Cenex Harvest States West Rehabilitated Bulkhead – Superior

The CHS West rehabilitated bulkhead is owned and operated by Cenex Harvest States. The bulkhead consists of a new steel sheet pile bulkhead with a metal cap. This new metal bulkhead was isolated from the previous steel sheet pile wall by the use of crushed stone and the tie back rods were isolated by being encased in concrete. This facility only sees low use by ships and is primarily used to retain the soil under the dock structure which supports the grain bins next to the waterfront. These bins are used for the storage of different grain products which are exported. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. Only aggressive corrosion of the mill scale was noted at the site.

Site 17- Cutler Magner Bulkhead – Superior

The Cutler Magner bulkhead is owned and operated by Cutler Magner. The bulkhead consists of a steel sheet pile bulkhead with a metal cap. This facility only sees moderate use for the import of Limestone and Coal materials. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans, instantaneous water quality measurements and instantaneous corrosion measurements. This site was fitted with a coupon tray with coupons for measurements in 2007.

Site 18- Lakehead Boat Basin Galv Bulkhead- Duluth

The Lakehead Boat Basin is owned and operated by Joel Johnson. The bulkhead consists of a galvanized steel sheet pile bulkhead with a galvanized metal cap. This facility sees moderate use by both charter and private recreational boats. It is important to note that this dock is not believed to have been electrically isolated from the old steel dock during rehabilitation. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements.

Site 19- Lakehead Boat Basin Original Bulkhead- Duluth

The Lakehead Boat Basin is owned and operated by Joel Johnson. The bulkhead consists of a steel sheet pile bulkhead with a metal cap. This facility sees moderate use by both charter and private recreational boats. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. The general water depth was very shallow along the bulkhead inspected and perforations were present.

Site 20- Community Sailing Dock Bulkhead – Duluth

The Community Sailing Dock bulkhead is owned and operated by the City of Duluth and volunteers. The bulkhead consists of a steel sheet pile bulkhead with a metal cap. This facility sees very low use by sail boats and private recreational boats. The field data collection for this site included visual inspection and measurements of the corrosion present at elevations from IGLD to the mud line on the out pans and instantaneous water quality measurements. The general water depth was very shallow along the



bulkhead inspected.

Site 21- John Sherwin Vessel @ Fraser Shipyard - Superior

The Vessel John Sherwin is owned and operated by Interlake Steamship of Cleveland. The ship hull was constructed in 1958 with steel plate and then coated for corrosion protection. The field data collection for this vessel included visual inspection and manual pitting measurements of the corrosion present from the water line to the keel.

Site 22- William Irvin Vessel – Duluth

The Vessel William Irvin is owned by U.S. Steels Great Lakes Fleet and operated by the Duluth Entertainment and Convention Center. The ship hull was constructed in 1937 with steel plate and then coated for corrosion protection. The field data collection for this vessel included visual inspection and manual pitting measurements of the corrosion present from the water line to the keel. It is important to note the concentration of the pitting was higher along the bows keel than on the hull plate. The coating is wearing and will need replacement or touch up in the near future.

General Assessment of Visual and Corrosion Data

In general the data collected was consistent with the structures that had been previously inspected in the other areas of the harbor. It's important to note that previously measured corrosion in other investigations researched was always reported from the current waterline or from the top of dock, not IGLD, which is the zero depth and reference for this study. With the water levels being much lower than what has been seen over the past years, the excessive pitting noted in the past is closer to the visual surface. This is very evident when you look at the high water marks on the structures around the harbor. Additionally the mussel population was thriving and present up higher on the sheet pile structures this year due to the mild ice season during the past winter.

The general conditions seen at most sites within the harbor are as follows:

0 to 0.5 feet below IGLD

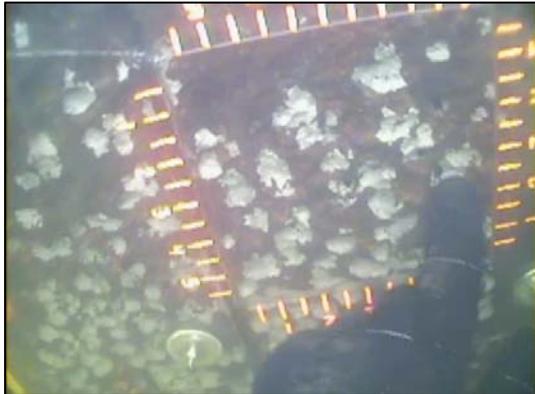
Generally the full material thickness remains with a lower severity of pitting.





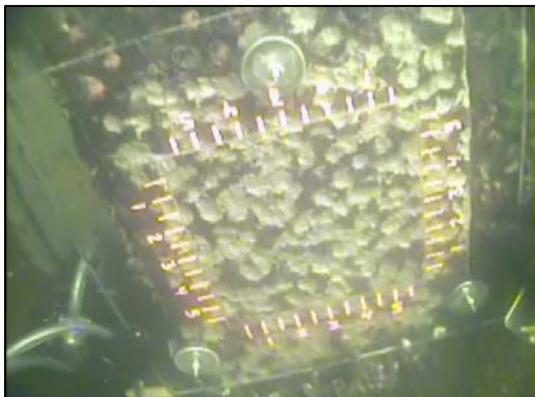
0.5 to 3 feet below IGLD

Uniform material thickness losses. High concentration and very deep scoop type pitting present. Perforation is present on sheet piling 3/8" or less in thickness that is 30 years or older.



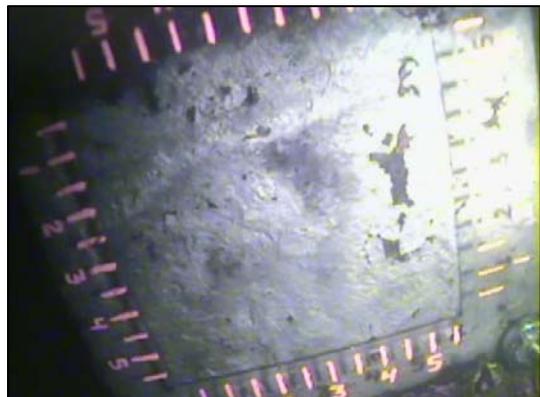
4 to 10 feet below IGLD

Uniform material thickness losses. High concentration of pitting over the entire surface with a transition from deep to shallow scoop type pitting from 4 to 10 feet. Large pitted areas tend to have numerous small 1/16 to 1/8 inch diameter pits within the larger pitted area.



10 to 32 feet below IGLD

Minor uniform material thickness losses. High to moderate very small concentrated pitting which tends to reflect more of an overall etched surface than actual pitting. In most areas the mill scale has been removed only and a very low concentration of actual deep pits existed.



It has been found in this Minnesota DNR funded study that the major differences in the degree of corrosion and type occurred as we inspected sites towards the Duluth entry and at the area at the CN Dock in Two Harbors. Both areas tend to see more flushing of fresh water than the general harbor area. The two harbors dock being the most unusual with large masses of the orange nodule type material v.s. individual orange nodules as found in the main Duluth/Superior Harbor.



Water Quality

Water Quality measurements were collected utilizing the Quanta Probe by Hydrolab. The probe was outfitted to take measurements that included depth, PH, Dissolved Oxygen, Conductivity, Turbidity, Temperature, Oxygen Reduction Potential (ORP) and Salinity at a few sites. Certain parts of the probe were calibrated at the factory and then individual site measurements based on the local barometric readings were added each day. Data for each site was taken at the time of the underwater inspections, but prior to the disturbance of the natural water conditions due to the cleaning and movement of the diver. Bulk water sample data was collected under the ACOE contract at a different date and time for all federal and non-federal structures. AMI assisted Altech Environmental in the collection of all bulk water samples. AMI is waiting for the release of this data by the ACOE for use in the non-federal study portion of the project.

Measured ranges for the data collected in July 2006 are as follows:

Temperature: 49° to 85° F

PH: 7.55 to 9.41

Dissolved Oxygen: 4.46 to 11.68 mg/L

Conductivity: 0.102 to 0.258 mS/cm

Turbidity: 1.7 to 48.6 NTU

ORP: 220 to 506 mV

Salinity: 0.06 to 0.08 PSS



The notable changes in water quality occurred at the measurements made at Two Harbors and at the hypothetical harbor East / West border at the Blatnick Bridge. Areas of water quality to the West of the Blatnick Bridge (St Louis Bay, Howard's Bay and up river to Oliver Bridge) had consistently higher water temperatures, PH, Conductivity, and ORP with lower dissolved oxygen readings. The measurement areas of the lower harbor were relatively constant from the Duluth to the Superior sites. The Two Harbors site had lower water temperature, conductivity and ORP with higher dissolved oxygen readings.

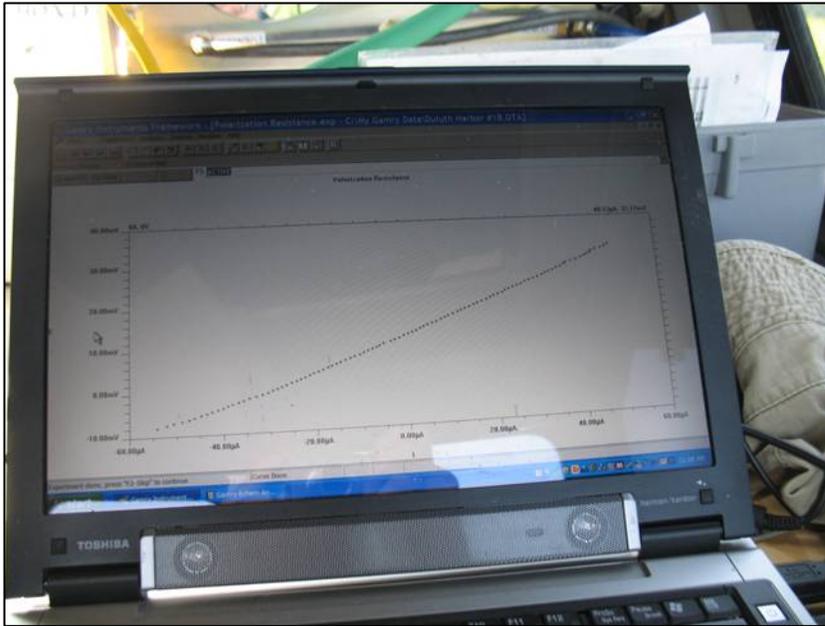
Linear Polarization Resistance Measurements

Linear Polarization Resistance (LPR) is probably the most common test method used in assessing the corrosiveness of an environment with respect to a metal. It is both relatively simple to perform, given the right computer driven test equipment, and provides reproducible results.

AMI Consulting Engineers hired corrosion experts Bushman & Associates (B&A) to assist AMI in performing the LPR tests and provide professional assessment of the results for the critical preselected sites throughout the harbor. AMI installed 6 out of 8 LPR test probes at the preselected locations on August 23, 2006 and LPR test probe #7



on August 29th, 2006. On September 7th, 2006, AMI and B&A proceeded with the first round of LPR measurements in the Duluth / Superior Harbor. These measurements were taken at the height of the typical corrosion rate season where we would typically see the most sunlight and highest water temperature readings. At the end of each computer controlled scan, the average corrosion rate for the test probe being scanned in the water was calculated. See Table 1 for the average corrosion rates. Since underground and submerged metal corrosion is almost always of the pitting type, it is common practice to multiply this average rate shown by a factor of 5, 10 or 20 to determine the pitting or perforation rate that can be expected. B&A often uses a rate of 7.5 times the average rate as a reasonable approximation of the pitting rate.



Resistance measurements are displayed on laptop screen.



One of the probes is visually inspected prior to being reinstalled.



Location Description	Test Locate No.	Scan No.	LPR Probe Ser. No.	Corrosion Rate (mpy)
Oliver Bridge	1	A	Ser. No. 06-98-1005	4.167740
Oliver Bridge	1	B	Ser. No. 06-98-1005	5.750072
Oliver Bridge	1	C	Ser. No. 06-98-1005	5.554085
Oliver Bridge	1	D	Ser. No. 06-98-1005	5.941934
Hallett 7 Dock	2	A	Ser. No. 06-08-1003	5.400351
Hallett 7 Dock	2	B	Ser. No. 06-08-1003	5.207576
Hallett 7 Dock	2	C	Ser. No. 06-08-1003	5.403211
Hallett 5 Dock	3	A	Ser. No. 06-08-1007	6.367826
Hallett 5 Dock	3	B	Ser. No. 06-08-1007	6.209100
Hallett 5 Dock	3	C	Ser. No. 06-08-1007	6.494123
Midwest Energy Dock	4	A	Ser. No. 06-08-1008	6.065133
Midwest Energy Dock	4	B	Ser. No. 06-08-1008	6.185771
Midwest Energy Dock	4	C	Ser. No. 06-08-1008	6.031089
DSPA Berth 4	5	A	Ser. No. 06-08-1004	4.030746
DSPA Berth 4	5	B	Ser. No. 06-08-1004	3.699939
DSPA Berth 4	5	C	Ser. No. 06-08-1004	4.014178
US Army COE Duluth Entry	6	A	Ser. No. 06-08-1006	1.977549
US Army COE Duluth Entry	6	B	Ser. No. 06-08-1006	2.165742
US Army COE Duluth Entry	6	C	Ser. No. 06-08-1006	2.012401
Superior Cutler Magner	7	A	Ser. No. 06-08-1009	4.541889
Superior Cutler Magner	7	B	Ser. No. 06-08-1009	4.641087
Superior Cutler Magner	7	C	Ser. No. 06-08-1009	4.496408

Table 1: September 7, 2006 LPR Measurements

Later in the year on October 17, 2006 an 8th LPR probe was added at the Superior Entry to provide complete coverage of the harbor. The second round of LPR measurements represents the corrosion rate over a longer period of time from the height of the normal corrosion potential in late August to the time of measurement just before the harbor started to freeze up on November 28th, 2006. Table 2 on page 15 shows the results from this longer period of LPR probe exposure. Looking at the data from both the short term at the height of the normal expected corrosion potential and the longer term data over a period of change from warm to cooler weather in the harbor, we start to generate information on the time periods maximum potential and a more average rate through the changes from a warm to colder weather conditions. Multiplying the average of rates measured for each location by 7.5 for the Short Term values in Table 1, we get the following pitting corrosion rates in mpy.

Oliver Bridge	40.15094	DSPA Berth 4	29.36216
Hallett 7	40.02785	USACOE Duluth Entry	15.38923
Hallett 5	47.67762	Superior Cutler Magner	34.19846
Midwest Energy	45.70491		



Location Description	Test Locate No.	Scan No.	LPR Probe Ser. No.	Corrosion Rate (mpy)
Oliver Bridge	1	A	Ser. No. 06-98-1005	0.641771
Oliver Bridge	1	B	Ser. No. 06-98-1005	0.649696
Oliver Bridge	1	C	Ser. No. 06-98-1005	0.644368
Hallett 7 Dock	2	A	Ser. No. 06-08-1003	1.200194
Hallett 7 Dock	2	B	Ser. No. 06-08-1003	1.203105
Hallett 7 Dock	2	C	Ser. No. 06-08-1003	1.199111
Hallett 5 Dock	3	A	Ser. No. 06-08-1007	2.419158
Hallett 5 Dock	3	B	Ser. No. 06-08-1007	2.491389
Hallett 5 Dock	3	C	Ser. No. 06-08-1007	2.687911
Midwest Energy Dock	4	A	Ser. No. 06-08-1008	2.352064
Midwest Energy Dock	4	B	Ser. No. 06-08-1008	2.370468
Midwest Energy Dock	4	C	Ser. No. 06-08-1008	2.304466
DSPA Berth 4	5	A	Ser. No. 06-08-1004	2.147834
DSPA Berth 4	5	B	Ser. No. 06-08-1004	2.119015
DSPA Berth 4	5	C	Ser. No. 06-08-1004	2.122074
US Army COE Duluth Entry	6	A	Ser. No. 06-08-1006	0.871615
US Army COE Duluth Entry	6	B	Ser. No. 06-08-1006	0.881193
US Army COE Duluth Entry	6	C	Ser. No. 06-08-1006	0.884629
Superior Cutler Magner	7	A	Ser. No. 06-08-1009	1.755004
Superior Cutler Magner	7	B	Ser. No. 06-08-1009	1.752357
Superior Cutler Magner	7	B	Ser. No. 06-08-1009	1.722814
US Army COE Superior Entry	8	A	Ser. No. 06-08-1002	1.854376
US Army COE Superior Entry	8	B	Ser. No. 06-08-1002	1.782855
US Army COE Superior Entry	8	C	Ser. No. 06-08-1002	1.784687

Table 2: November 28, 2006 LPR Measurements

Multiplying the average of rates measured for each location by 7.5 for the longer term values in Table 2, we get the following pitting corrosion rates in mpy.

Oliver Bridge	4.83959	DSPA Berth 4	15.97231
Hallett 7	9.00602	USACOE Duluth Entry	6.59359
Hallett 5	18.99614	Superior Cutler Magner	13.07544
Midwest Energy	17.56749	USACOE Superior Entry	13.55480

Converting the longer term pitting corrosion rate numbers into inches per year we get a minimum rate of 0.005 inches per year to a maximum of 0.019 inches per year if this was representative of the entire year average rate. Over 30 years this converts to a pitting depth range of 0.15 to 0.57 inches, depending on the location in the harbor.

I feel it is important to note that the major changes that occurred during the time period from late August to November 28th, 2006 appear to be the cooler water temperatures



and the shorter days which represent less benefit from sunlight. In the summary of the initial workshop findings temperature was believed to not be significant, but we believe the data clearly shows a correlation between water temperature and corrosion rate.

Sample Tray Installation

After numerous meetings with the corrosion committee members, AMI designed a preliminary coupon sample tray. The initial discussions of the coupon tray design primarily revolved around the issue of isolation of the coupon materials from the existing steel walls. If the coupons were in contact directly to the existing corroding steel, it has been shown in other study's that the new metal will corrode faster than the existing steel due to the difference in electrical resistance. If the steel was isolated from the existing steel using a non-conductive material the concern is then the samples would not represent the sheet piling as it is grounded to the soil. After review and comments, it was found that through previous dive inspections on wood crib systems, patches that had been installed which were not directly grounded still corroded a similar manner to that of the sheet piling that is grounded. Due to this observation, the decision was made to isolate the samples from the existing steel using a non-conductive material. The coupon material utilized would be ASTM A328 steel material, which is the primary material used for hot rolled sheet piling.

The final tray design went through a few iterations. After determining the final position of the tray which would best serve the study and determining the final number of samples needed, a final design layout was determined and a prototype was constructed. The prototype served as a visual product to show all interested parties the working design and to determine the cost of fabrication. From this prototype, most of the fabrication bugs were worked out, a final fabrication cost was determined for budgeting and a final CAD layout was completed. See Appendix F for the final drawing of the tray. Seven trays were constructed by a local fabricator for installation.

It is planned that one or two samples will be taken out every six months at each site. These samples will be utilized to measure physical overall corrosion loss, provide in-situ biological growth for culturing and DNA testing and would be used to study the changes and affects of the corrosion on the steel samples themselves. The final installation site locations were determined by the committee to provide the most scientific benefit while providing the broadest range of coverage. Before each sample was installed in the trays at each site around the harbor they were carefully marked for future identification. After each sample was marked it was measured for size and very precisely weighed. A complete chart of the sample identifiers, sizes, numbers and dates of install can be found in appendix F. The samples were then installed in each sample tray and secured in place for future removal. Six of the seven sample trays were installed in 2006, with the seventh sample tray scheduled to be installed on the Superior Entry in 2007.

Summary

The previously reported corrosion conditions as discussed in the 2004 ACOE Document ERDC/CERL SR-05-3 on the Fresh Water Corrosion in the Duluth – Superior Harbor existed on the majority of the structures within the harbor confines. The major difference noticed during the corrosion inspections was at the CN Railway Dock in Two Harbors. Although some pitting, orange masses and corrosion was present, its visual appearance was different in many aspects. From the general harbor to the Oliver Bridge, typical characteristics of the corrosion were present with minor differences in marine growth,



size, pitting penetration and concentration.

The general penetration of the pitting within the 0 to 4 feet IGLD water level on all the facilities in the main harbor older than 30 years was typically 0.25 to 0.375 of an inch and most of the 0.375 inch sheet pile structures older than thirty years were close to being perforated or perforated from 1 to 3 feet below IGLD. Although the Oliver Bridge site is not in the general harbor confines, similar conditions existed on the steel structures, which were previously believed to not have been affected by the accelerated corrosion. The active levels of the accelerated corrosion problem were evident when looking at the newer steel sheet pile installed at Cenex Harvest States in 2003, with orange nodules covering over 50 to 75% of the sheet pile surfaces with measurable pitting size and penetration. The other sheet pile inspected in the Duluth Superior harbor less than 30 years old had a degree of uniform corrosion and pitting relative to its age. From the inspection data it appears that the corrosion rates, overall level of corrosion and pitting becomes less from the main harbor area towards Lake Superior through the Duluth Entry, but stays relatively consistent from the main harbor towards the Superior Entry.

The data from the areas investigated should be carefully evaluated before overall conclusions or claims are made pertaining to the accelerated corrosion issue. Although this information provides a good cross section of the general harbor, other areas not currently inspected could have different characteristics and degree of corrosion not previously discovered.

Respectfully Submitted:

Chad Scott, P.E.
AMI Consulting Engineers, P.A.

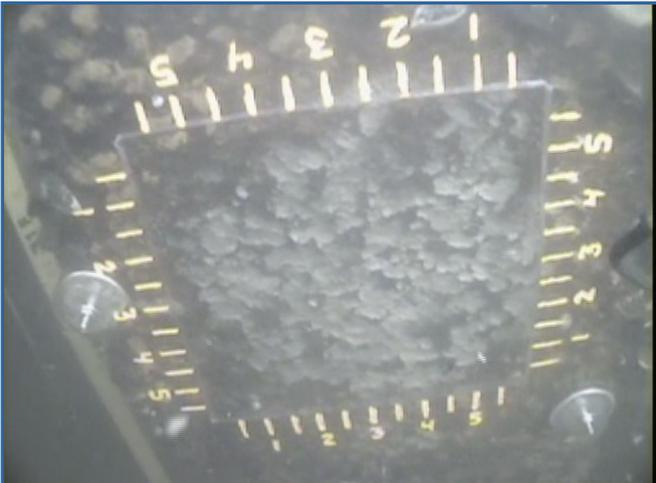


APPENDIX A

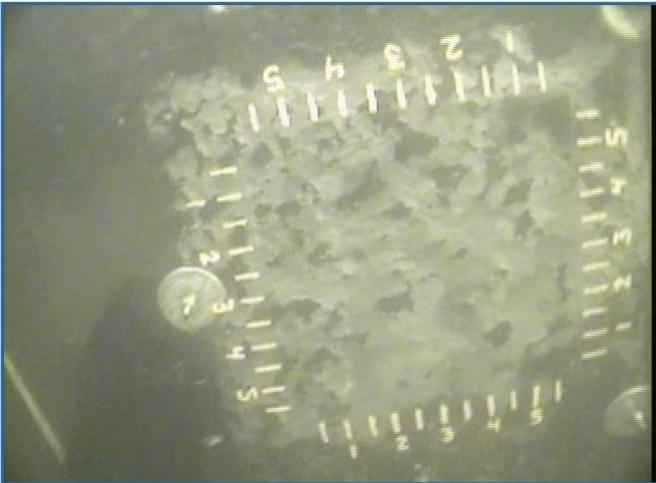
Photo Index



DSPA Berth 1- 0 feet

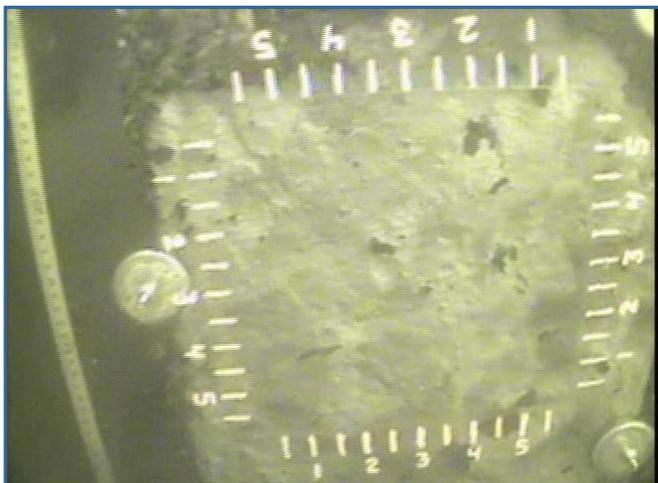


DSPA Berth 1- 2 feet

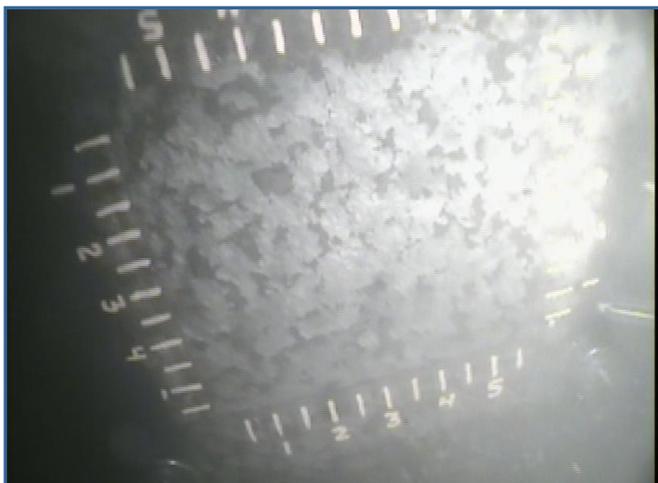


DSPA Berth 1- 4 feet

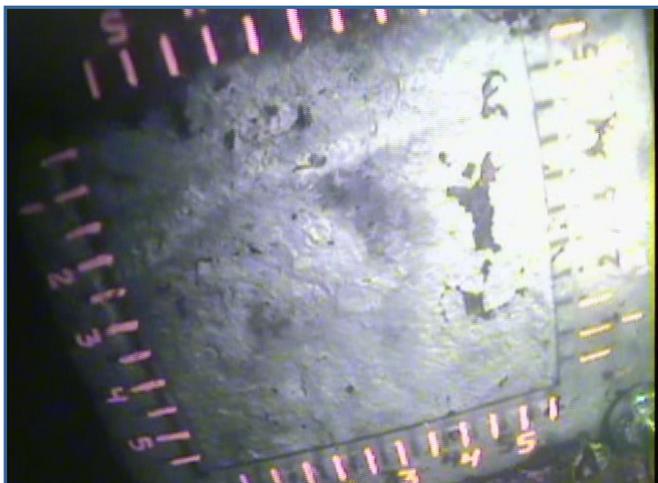




DSPA Berth 1- 6 feet

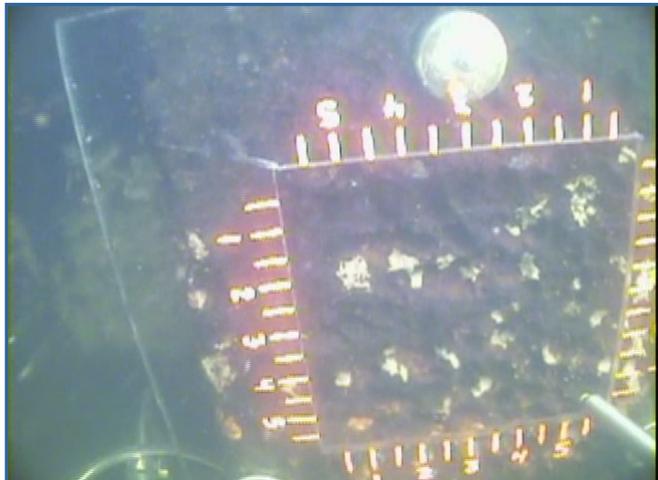


DSPA Berth 1- 8 feet

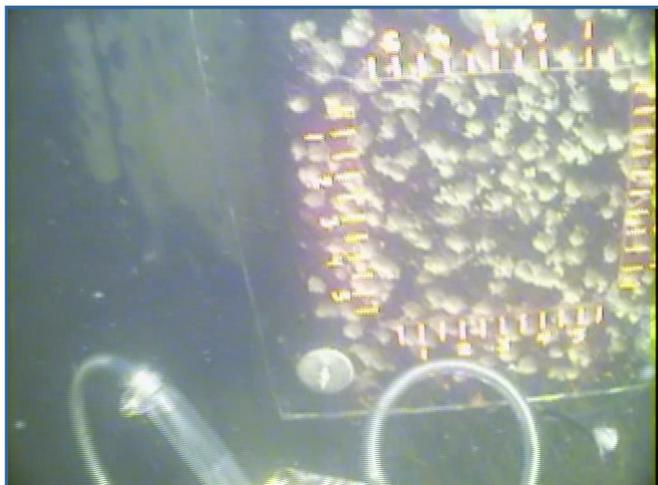


DSPA Berth 1- 10 feet

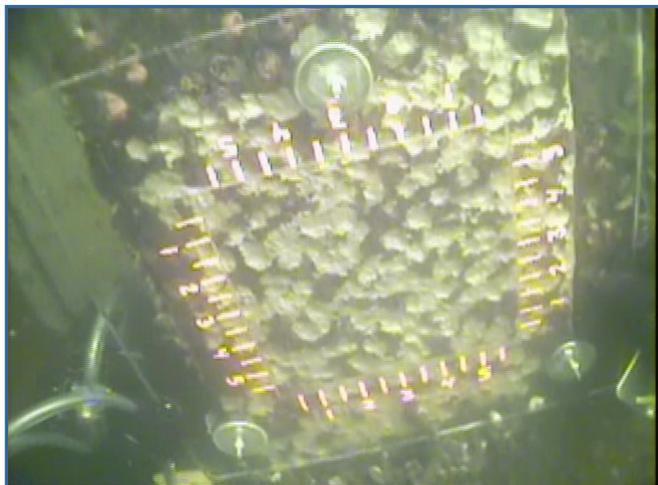




DSPA Berth 4- 0 feet

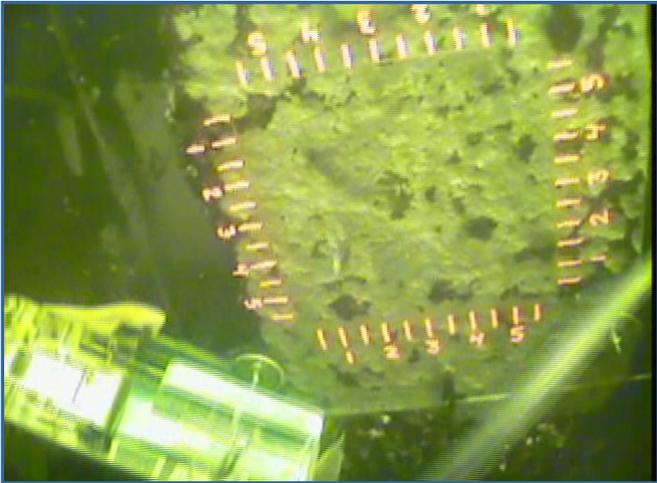


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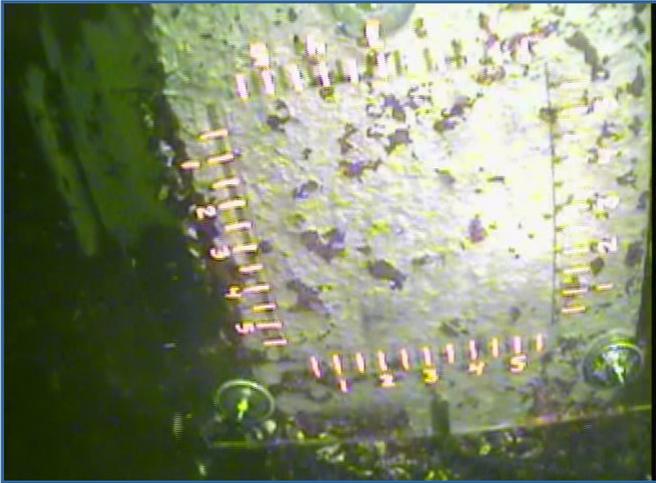


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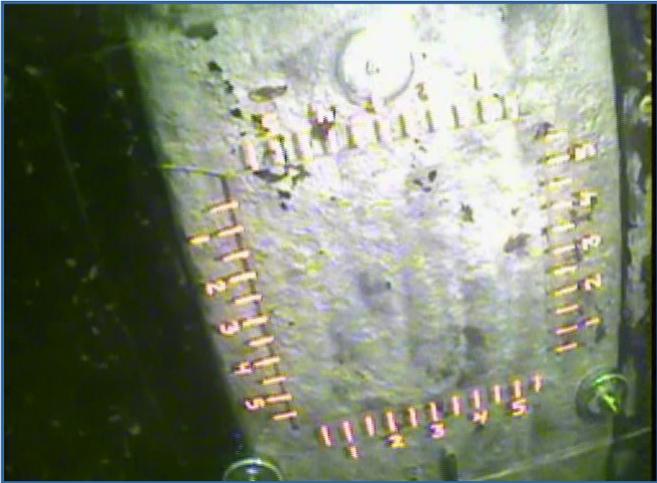




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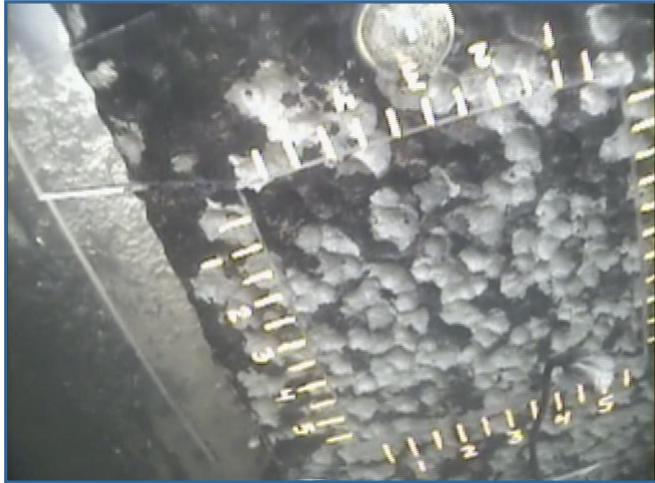


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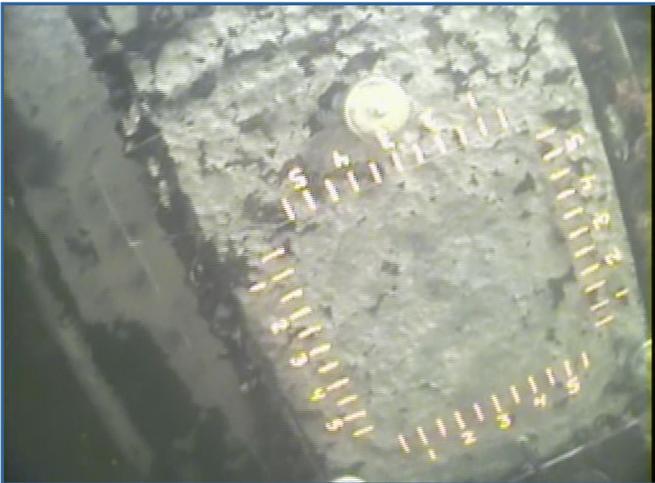


DSPA Berth 4- 10 feet

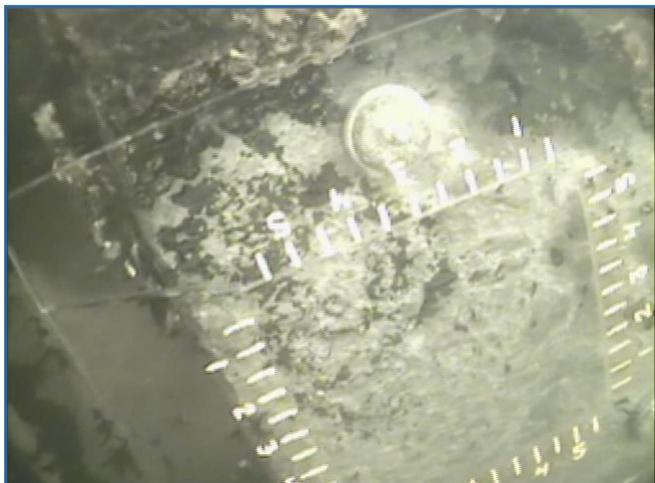




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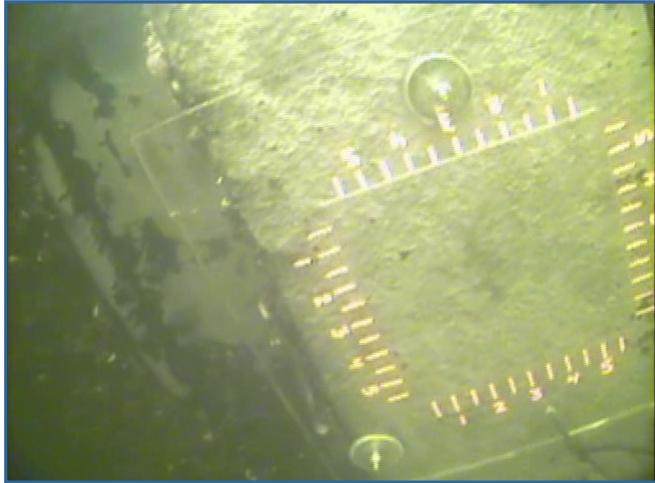


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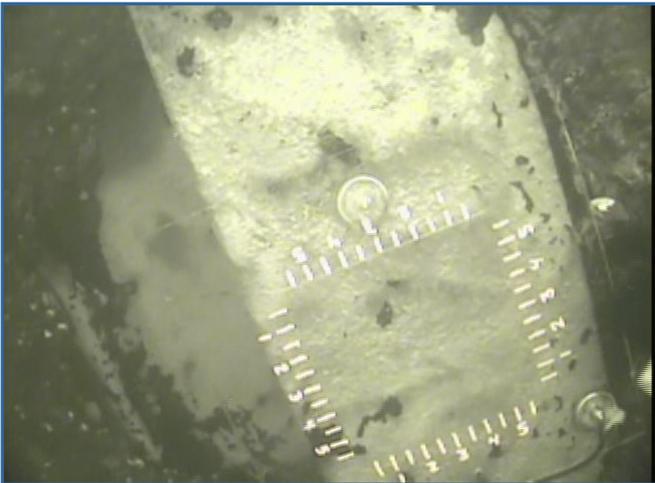


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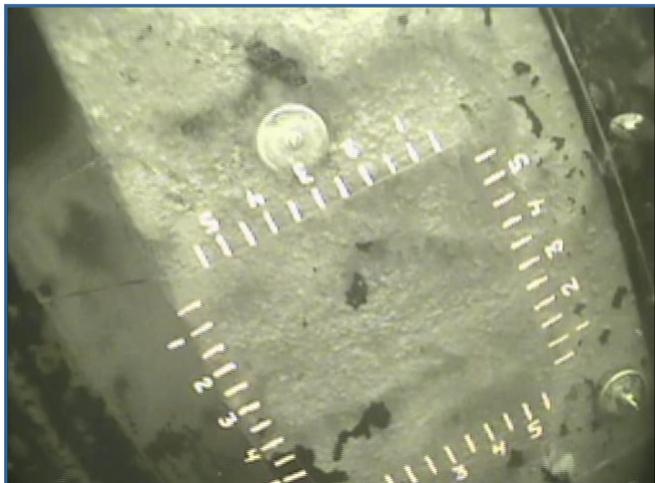




DSPA Berth 6- 6 feet



DSPA Berth 6- 8 feet



DSPA Berth 6- 10 feet

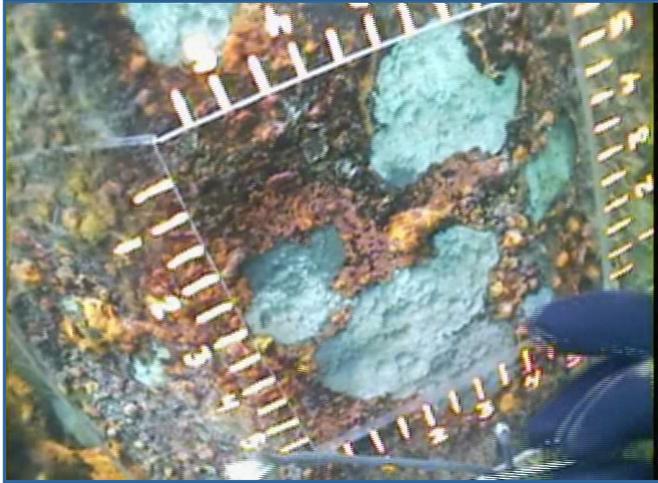




CN Two Harbors- 0 feet



CN Two Harbors- 2 feet

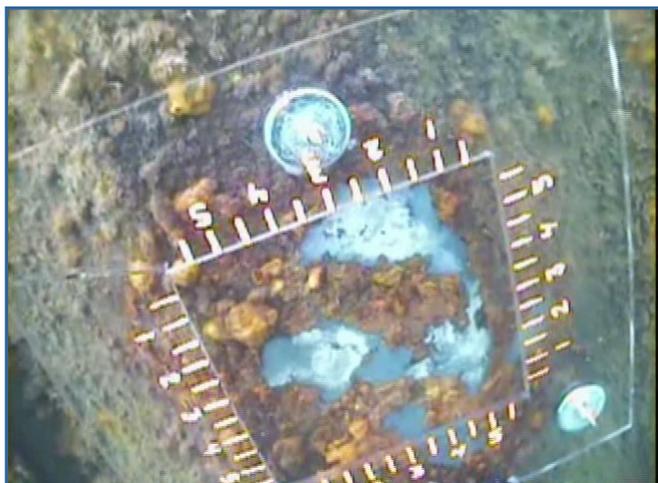


CN Two Harbors- 4 feet





CN Two Harbors- 6 feet

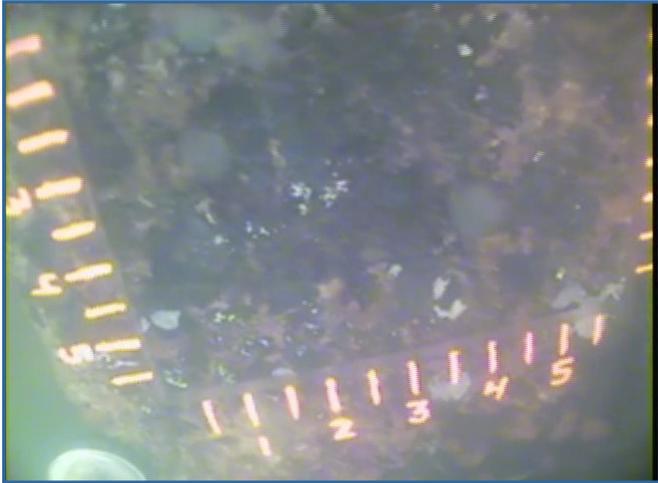


CN Two Harbors- 8 feet

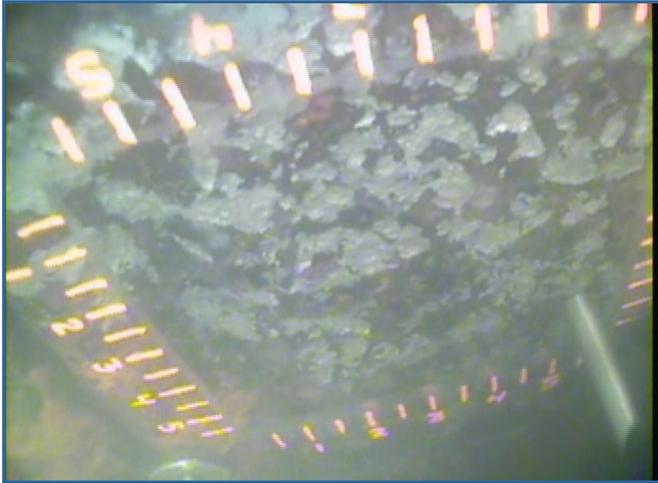


CN Two Harbors- 10 feet

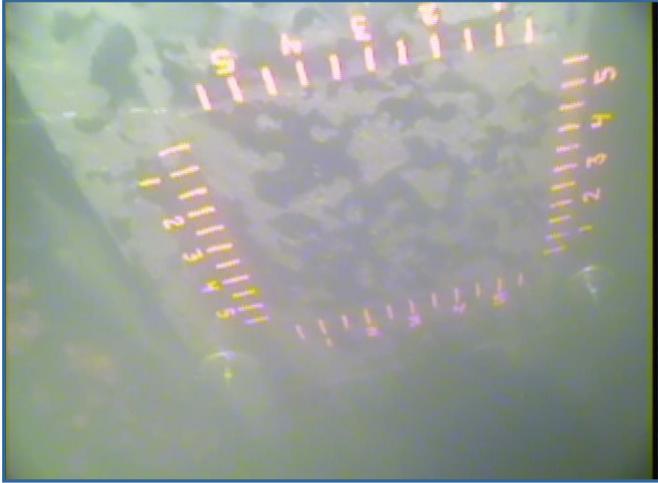




Minnesota Slip- 0 feet

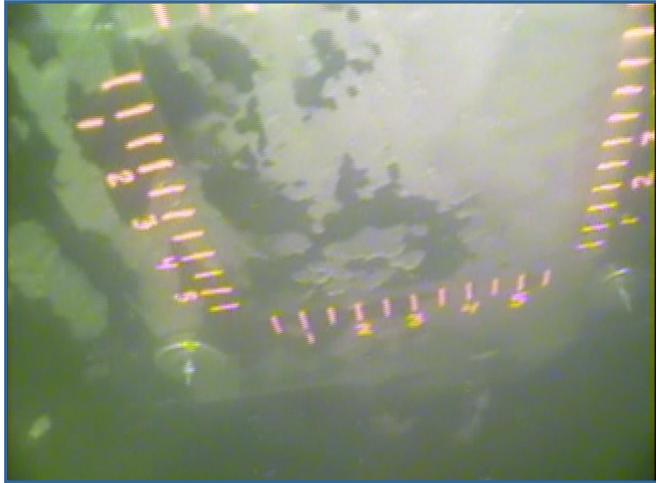


Minnesota Slip- 2 feet

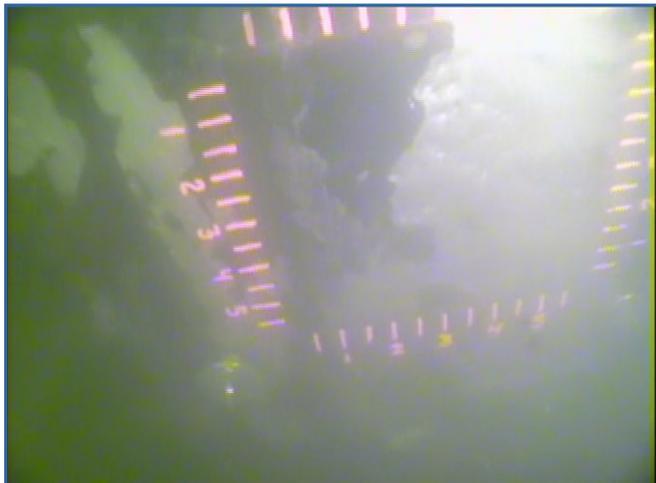


Minnesota Slip- 4 feet

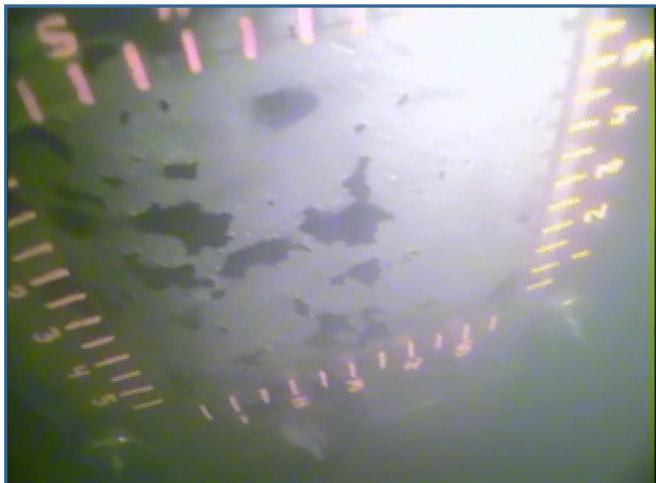




Minnesota Slip- 6 feet



Minnesota Slip- 8 feet

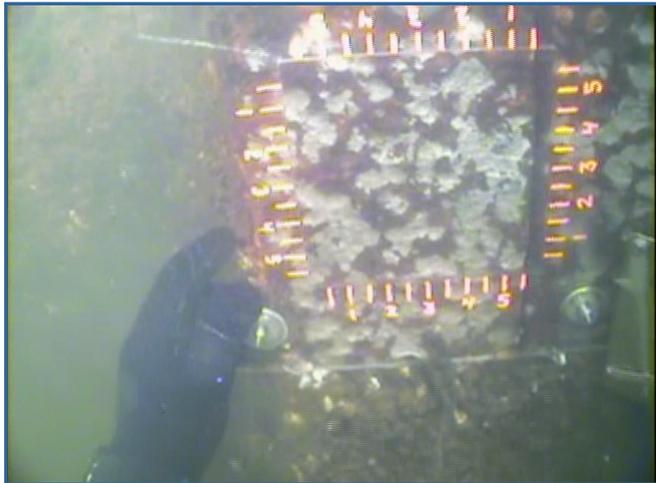


Minnesota Slip- 10 feet

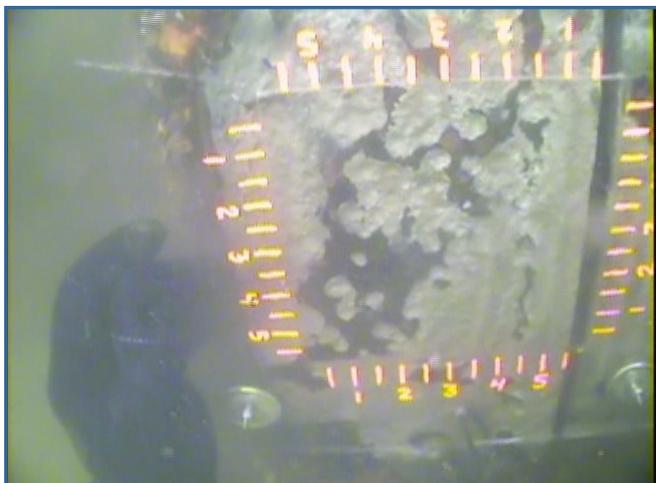




DECC Dock- 0 feet

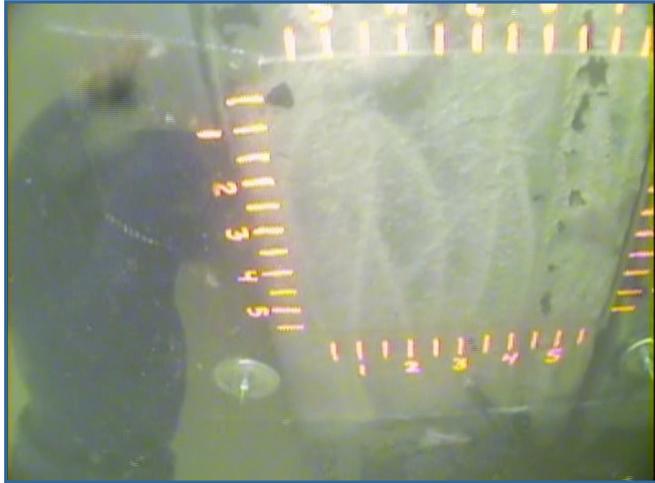


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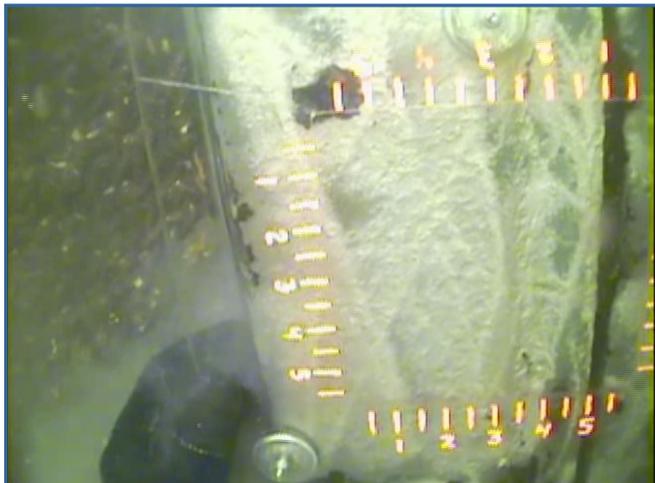


DECC Dock- 4 feet

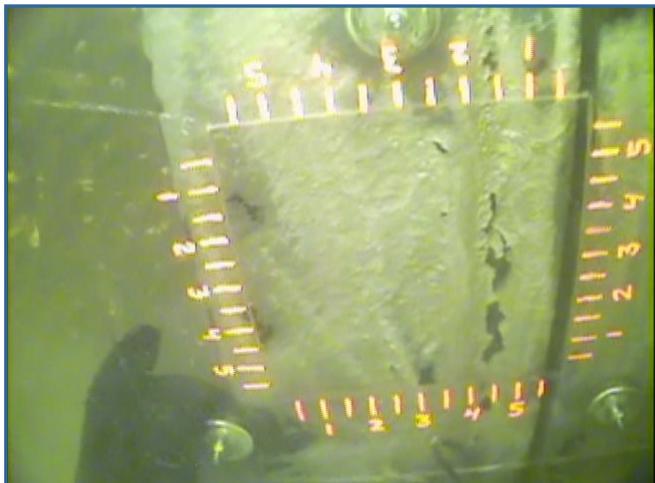




DECC Dock- 6 feet



DECC Dock- 8 feet

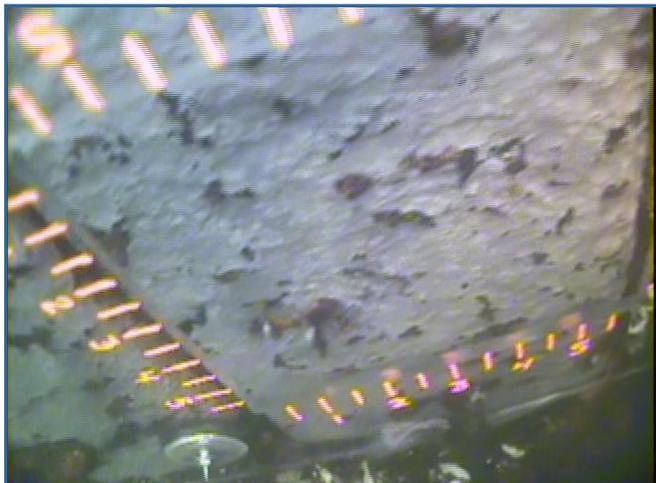


DECC Dock- 10 feet





CARGILL Dock- 0 feet

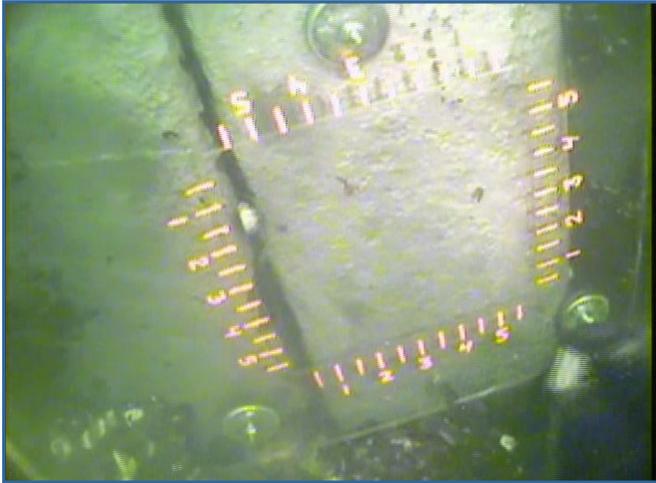


CARGILL Dock- 2 feet

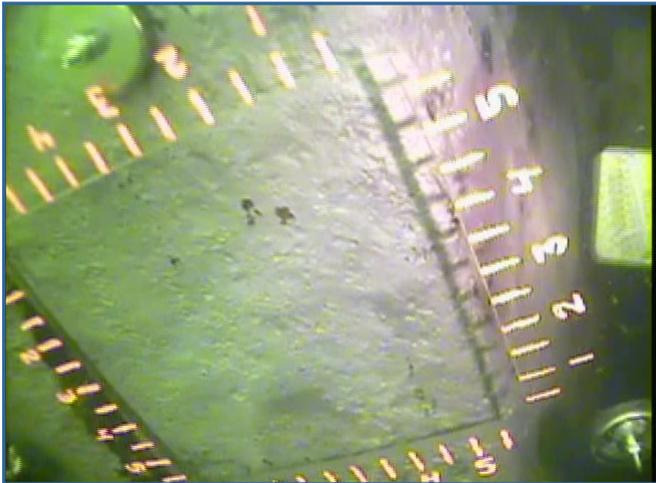


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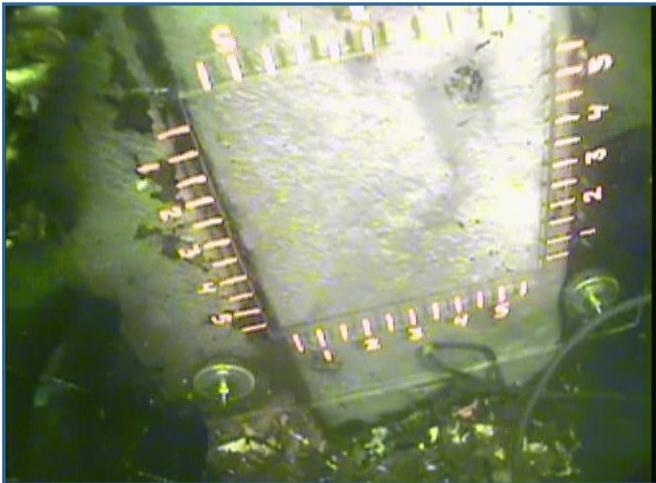




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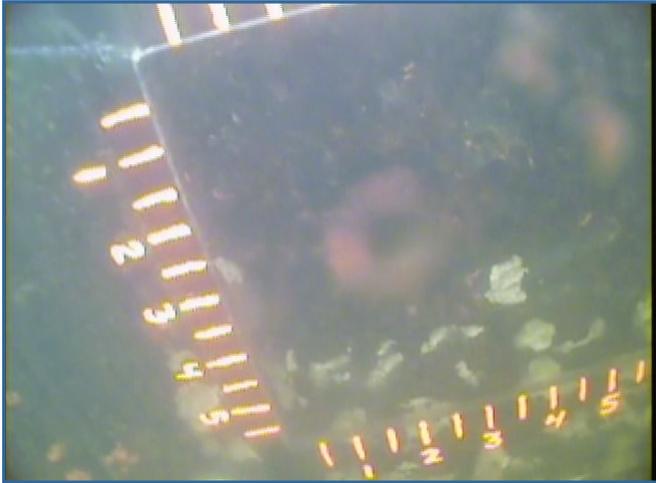


CARGILL Dock- 8 feet

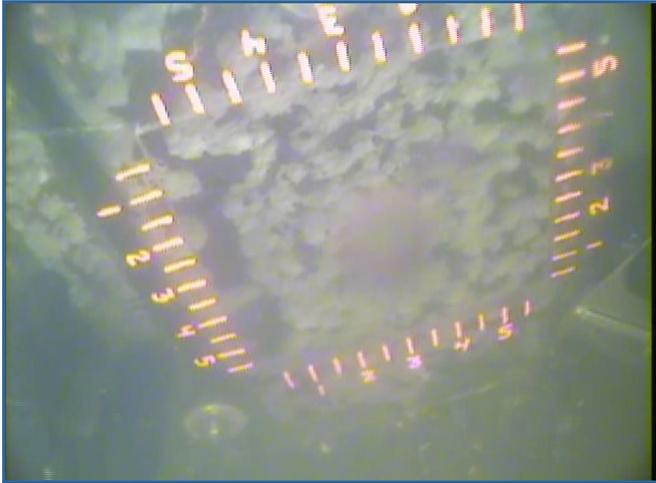


CARGILL Dock- 10 feet

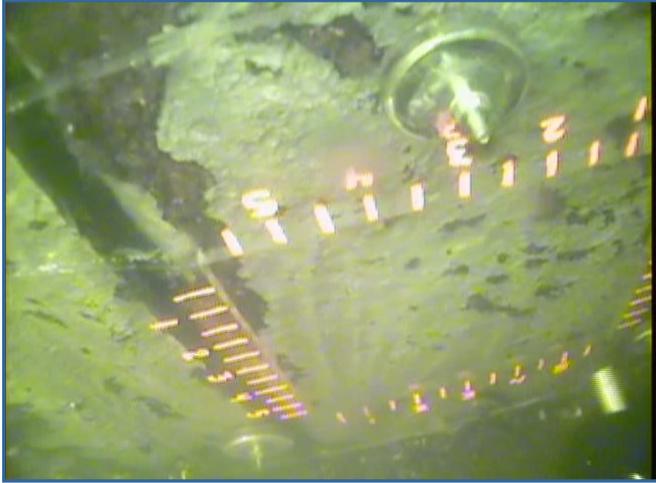




Hallett Dock 5- 0 feet



Hallett Dock 5- 2 feet

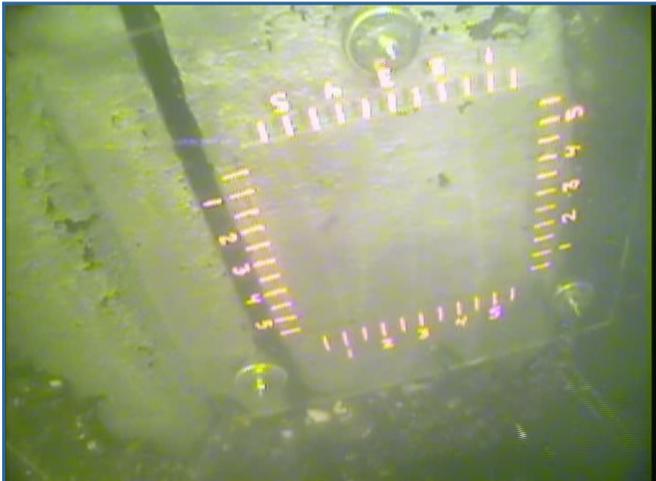


Hallett Dock 5- 4 feet

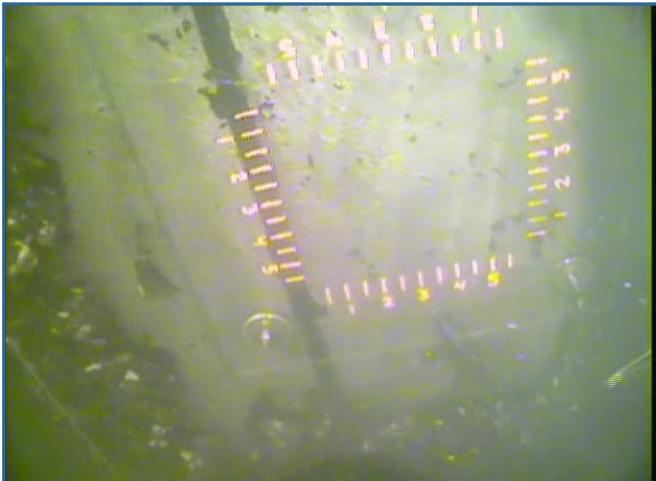




Hallett Dock 5- 6 feet

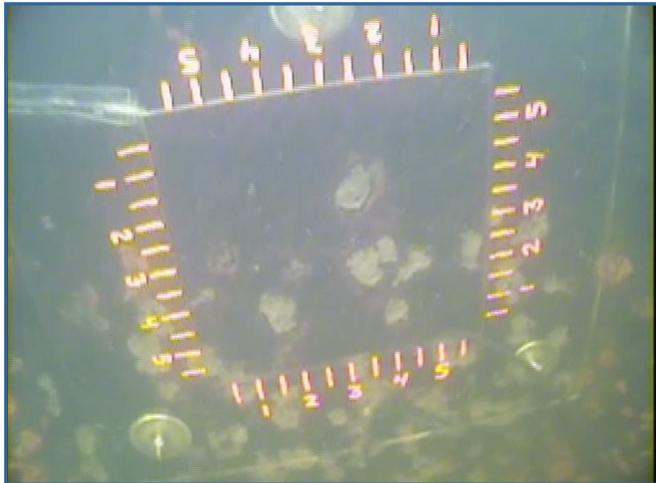


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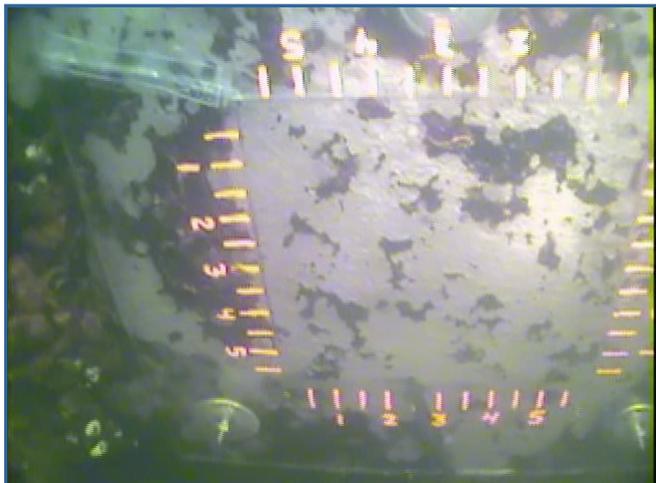


Hallett Dock 5- 10 feet





Bong Bridge Cell- 0 feet

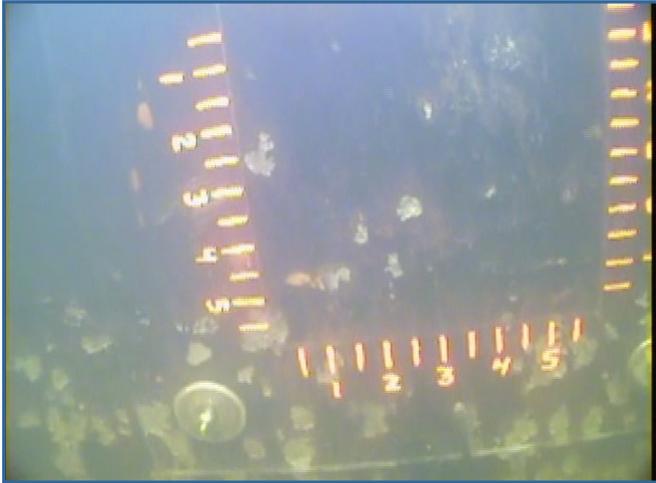


Bong Bridge Cell- 2 feet

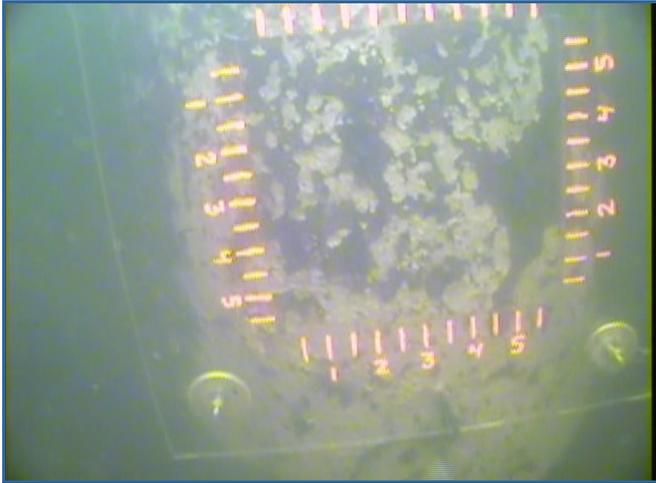


Bong Bridge Cell- 10 feet





Spirit Lake Marina- 0 feet

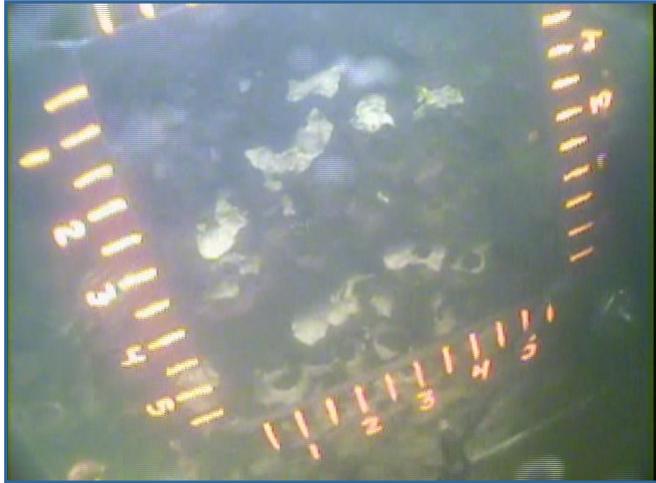


Spirit Lake Marina- 2 feet

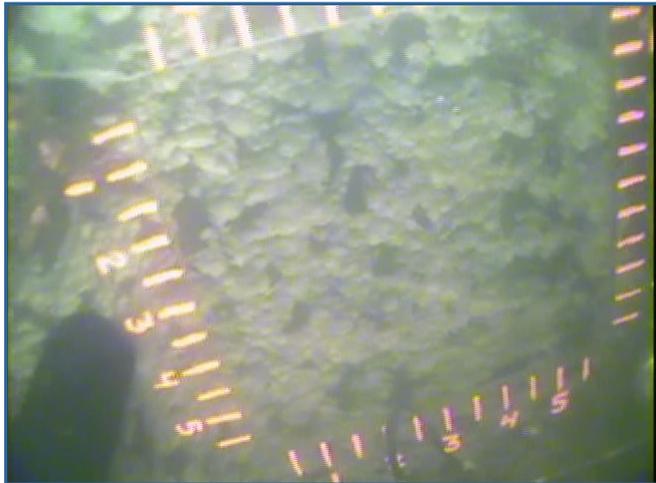


Spirit Lake Marina- 3 feet

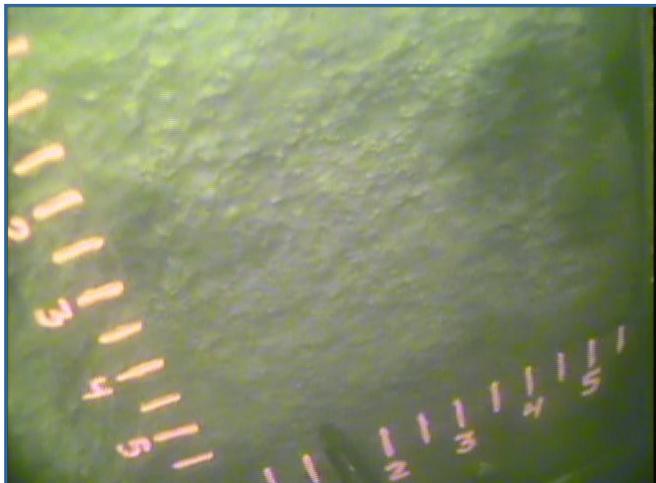




Oliver Bridge- 0 feet

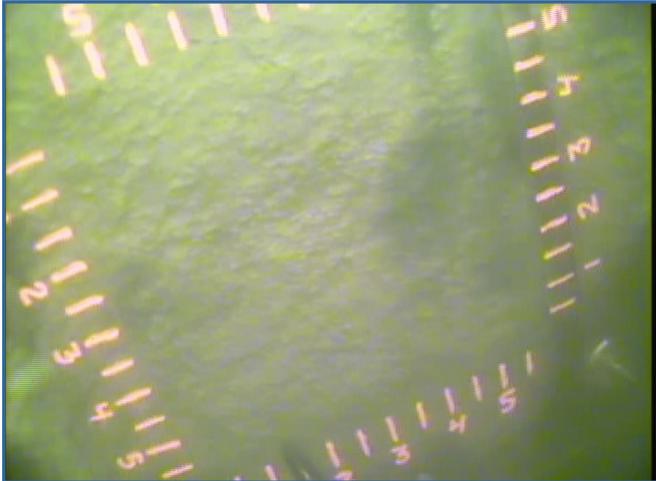


Oliver Bridge- 2 feet

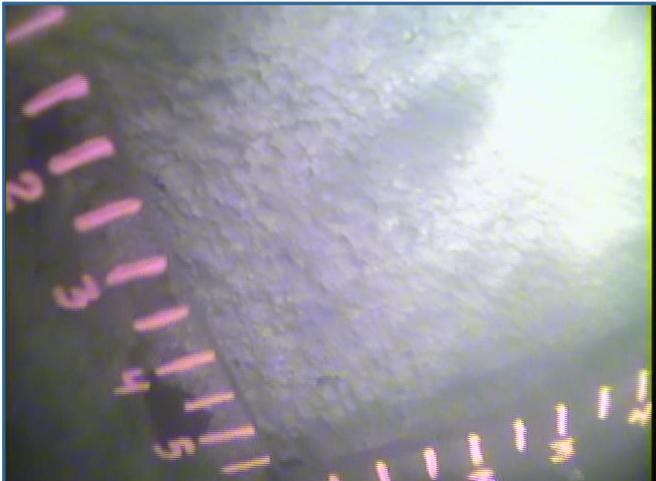


Oliver Bridge- 4 feet





Oliver Bridge- 6 feet

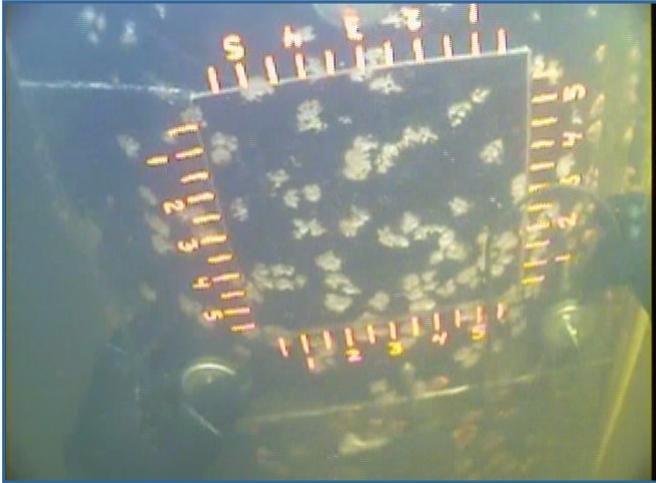


Oliver Bridge- 8 feet

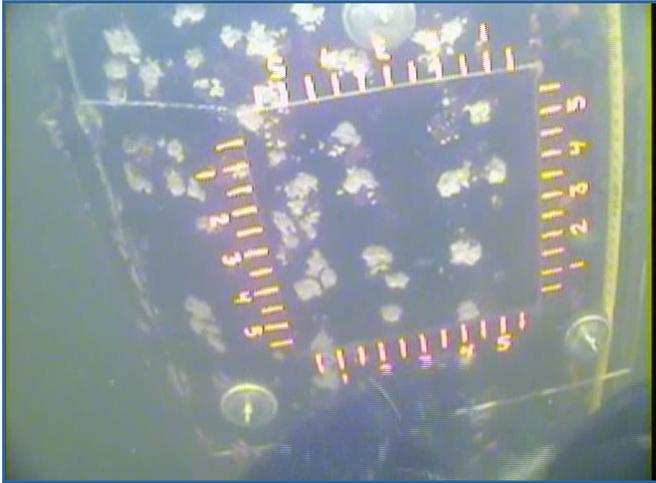


Oliver Bridge- 10 feet

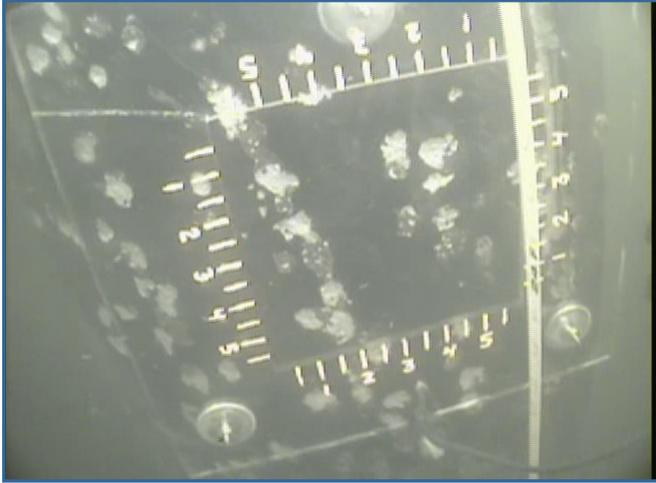




Midwest Energy (Pile w/ Jacket)- 0 feet



Midwest Energy (Pile w/ Jacket)- 2 feet



Midwest Energy (Pile w/ Jacket)- 4 feet

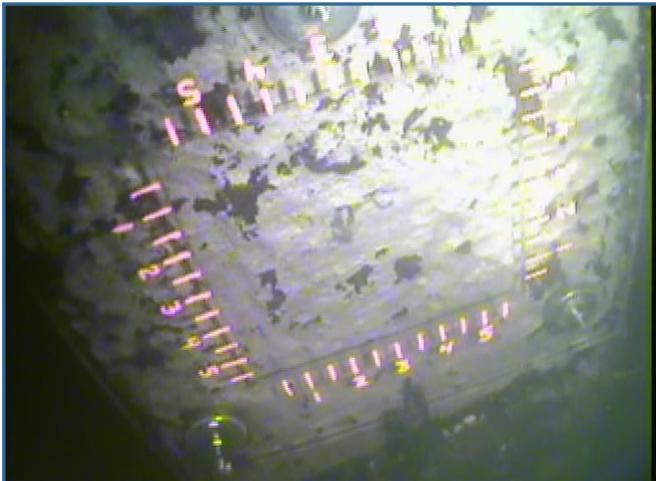




Midwest Energy(Pile w/ Jacket) - 6 feet

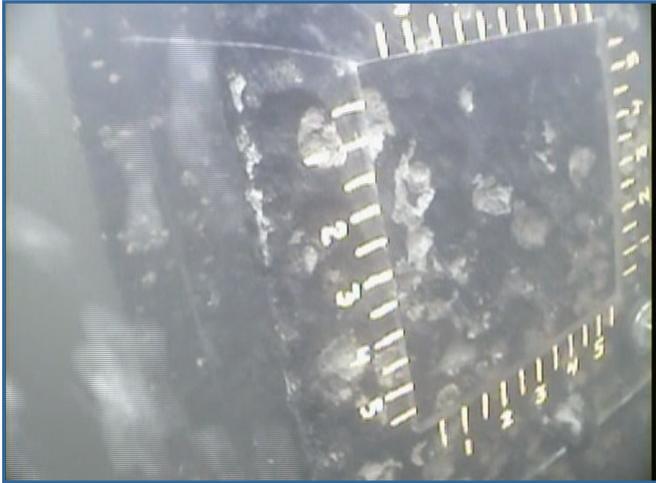


Midwest Energy(Pile w/ Jacket) - 8 feet

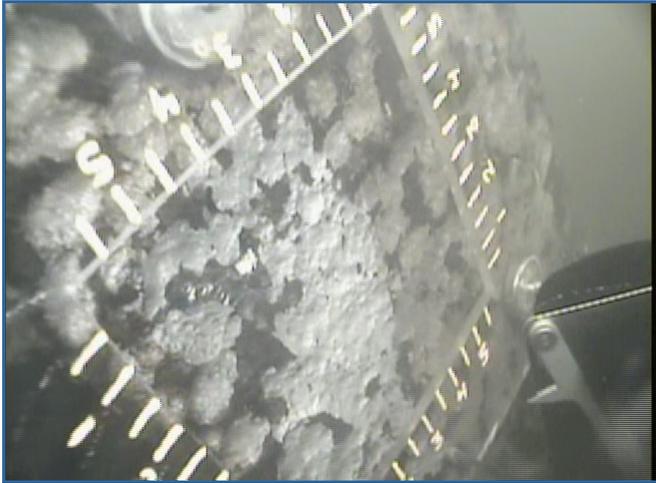


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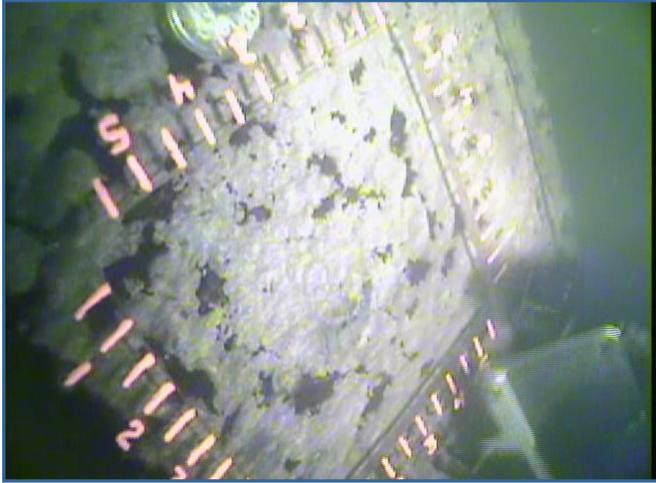




Midwest Energy (Pile w/o Jacket)- 0 feet



Midwest Energy (Pile w/o Jacket) - 2 feet

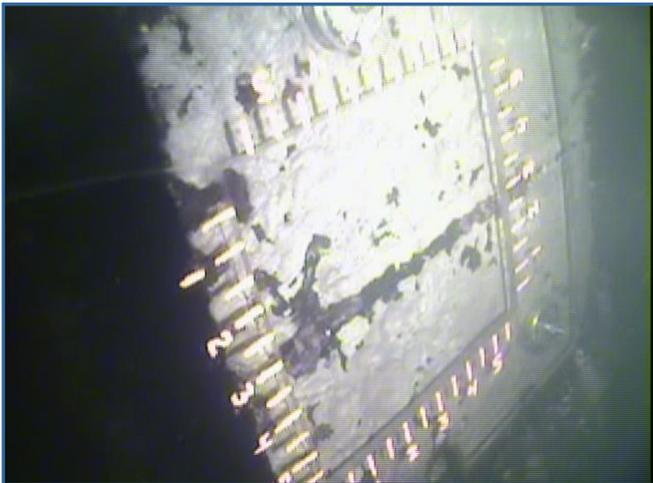


Midwest Energy (Pile w/o Jacket) - 4 feet

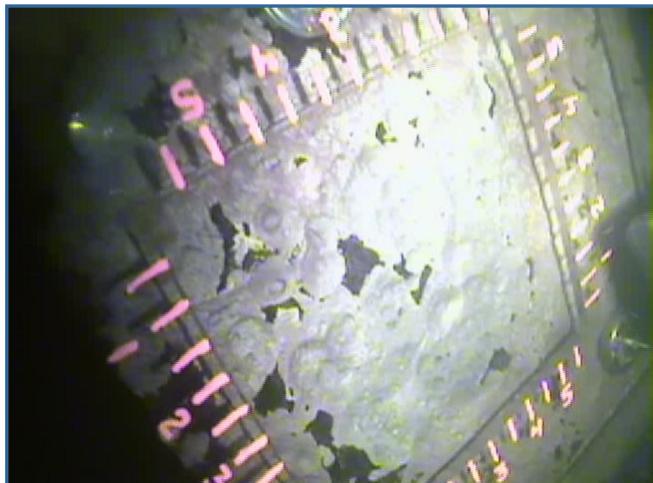




Midwest Energy (Pile w/o Jacket) - 6 feet



Midwest Energy (Pile w/o Jacket) - 8 feet

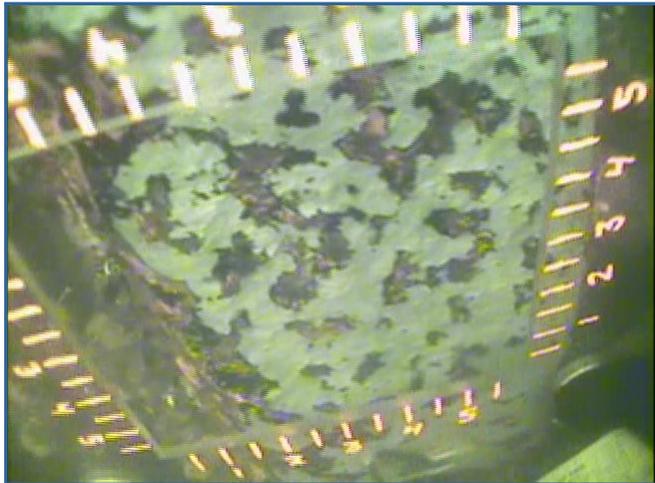


Midwest Energy (Pile w/o Jacket) - 10 feet

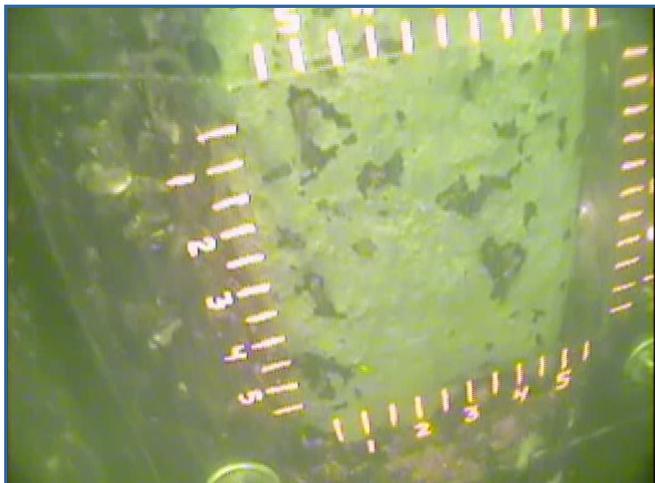




CHS 1- 2 feet

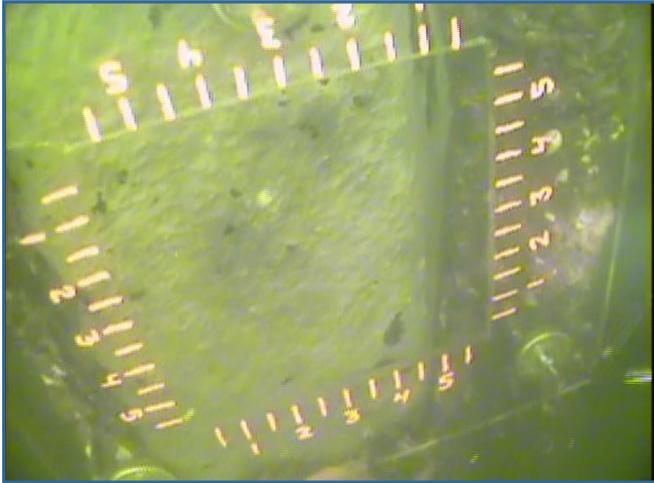


CHS 1- 4 feet

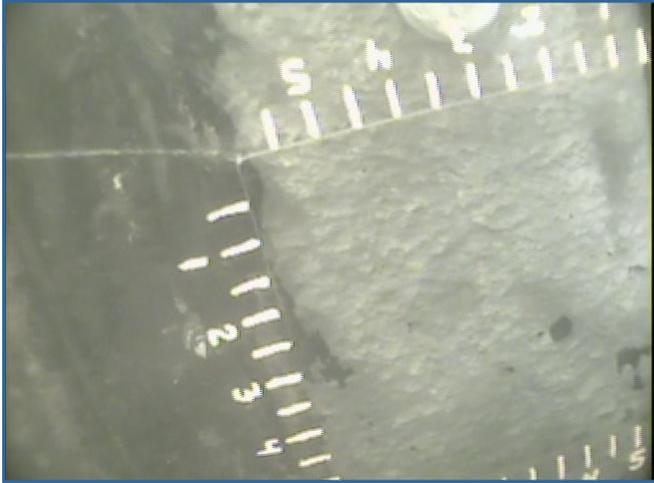


CHS 1- 6 feet





CHS 1- 8 feet

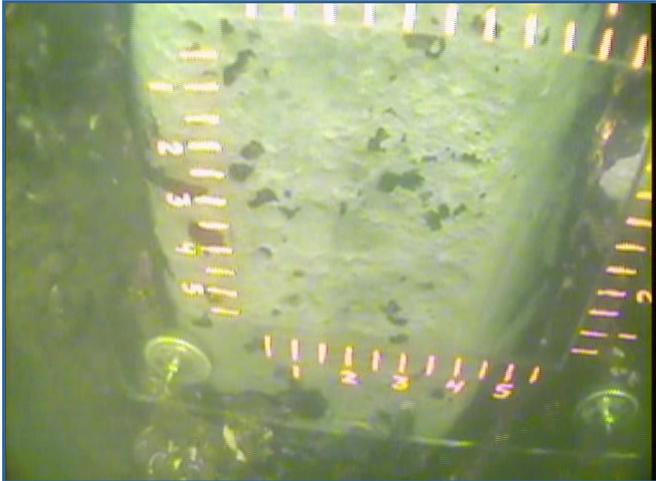


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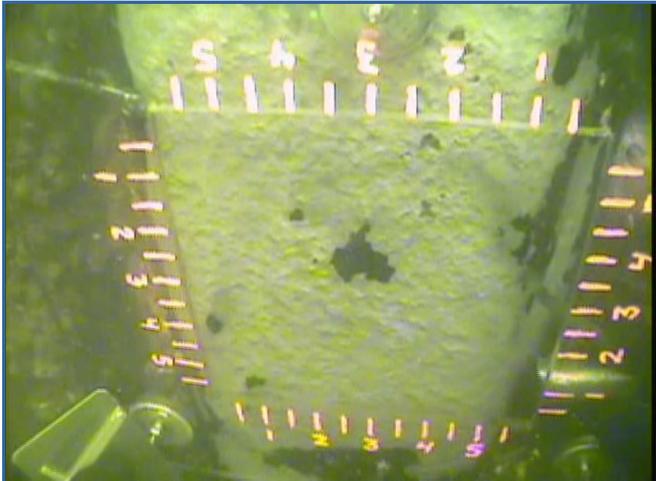




CHS 2- 2 feet



CHS 2- 4 feet

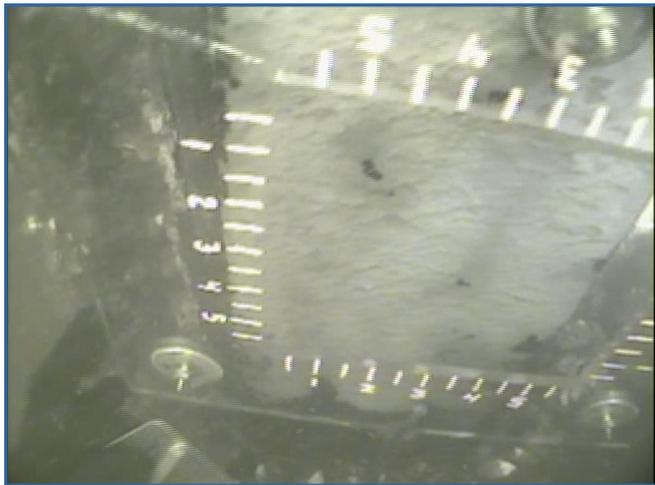


CHS 2- 6 feet

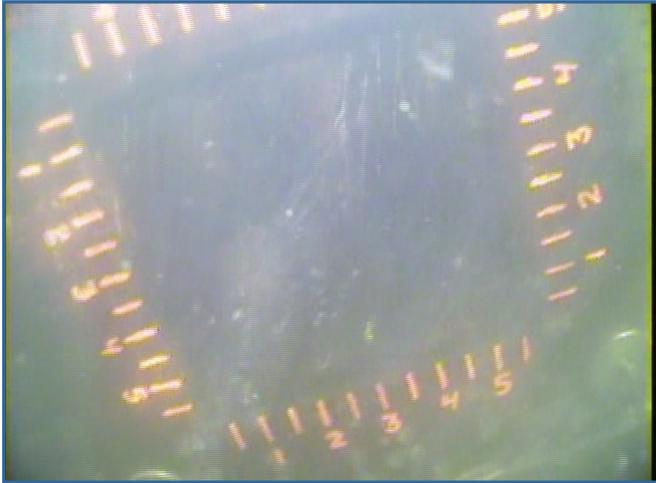




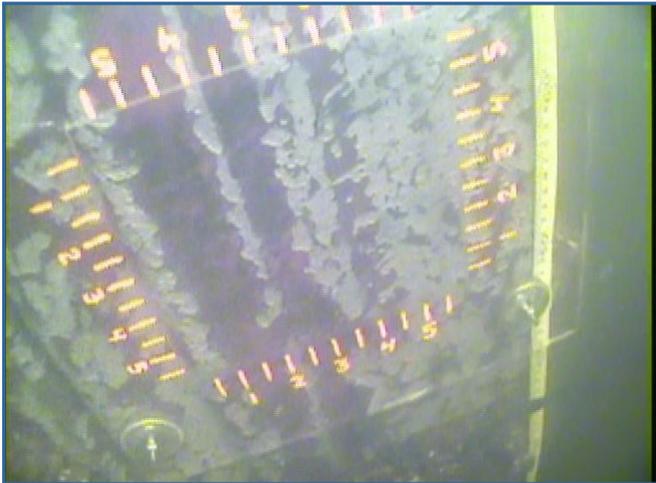
CHS 2- 8 feet



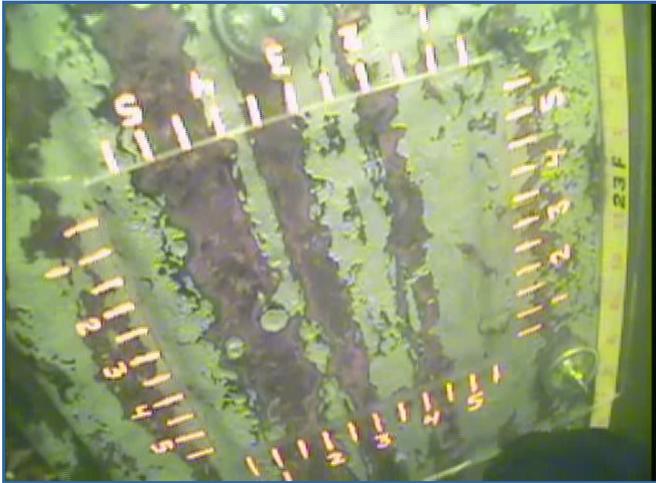
CHS 2- 10 feet



CHS 3- 0 feet

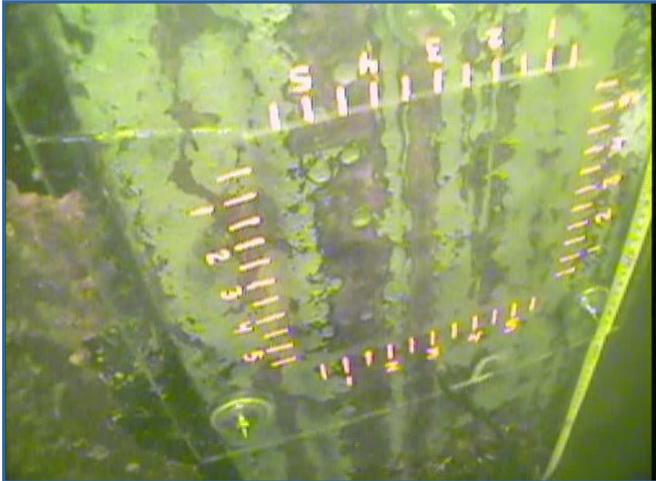


CHS 3- 2 feet



CHS 3- 4 feet

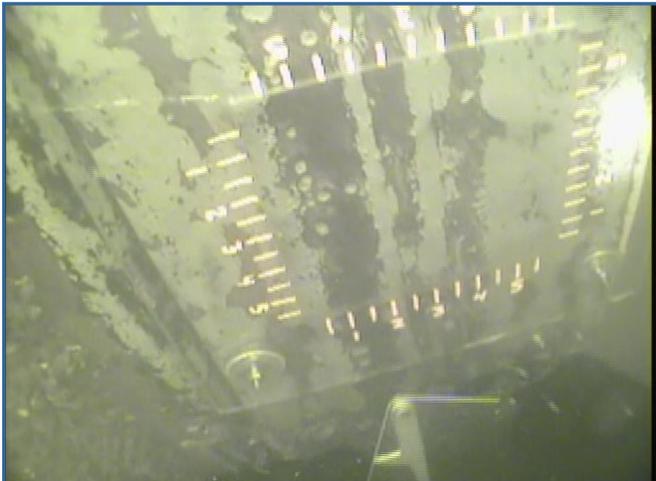




CHS 3- 6 feet

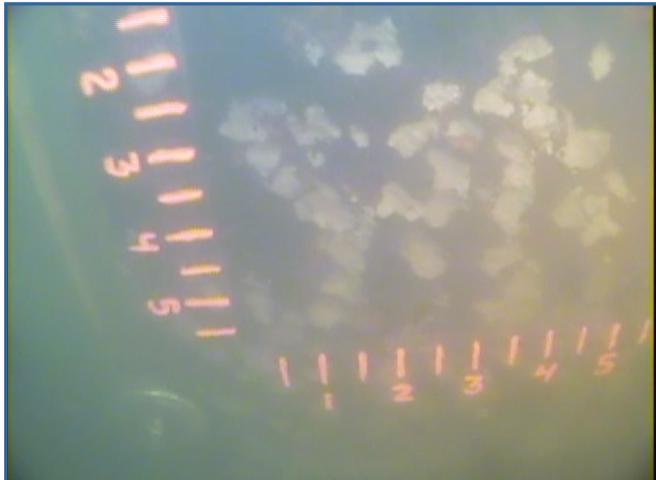


CHS 3- 8 feet

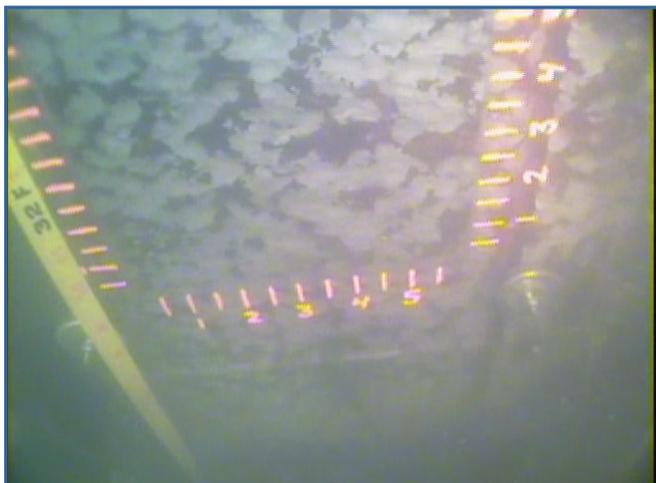


CHS 3- 10 feet





Cutler-Magner - 0 feet



Cutler-Magner - 2 feet



Cutler-Magner - 4 feet

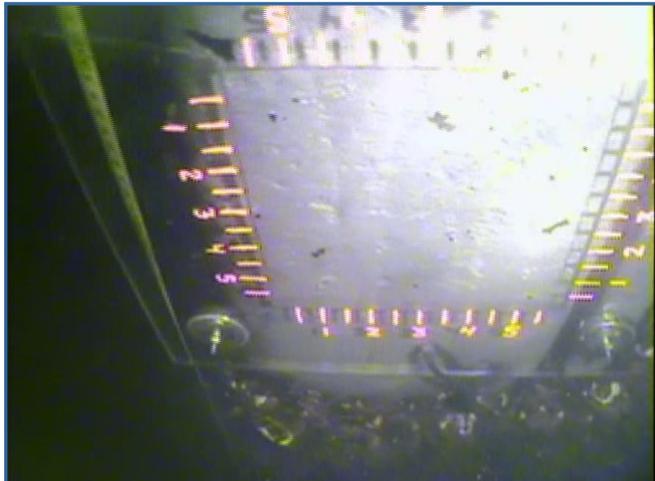




Cutler Wagner - 6 feet



Cutler Wagner - 8 feet

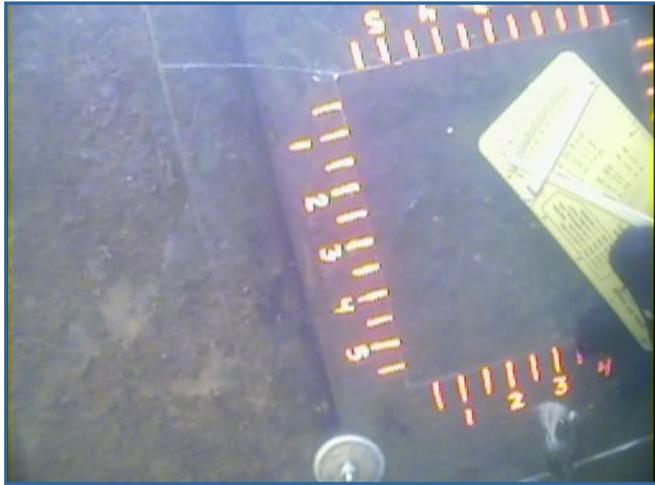


Cutler Wagner- 10 feet





Lakehead Boat Basin (galvanized sheet pile) - 0 feet



Lakehead Boat Basin (galvanized sheet pile) - 2 feet



Lakehead Boat Basin (galvanized sheet pile) - 4 feet





Lakehead Boat Basin (steel sheet pile) - 0 feet

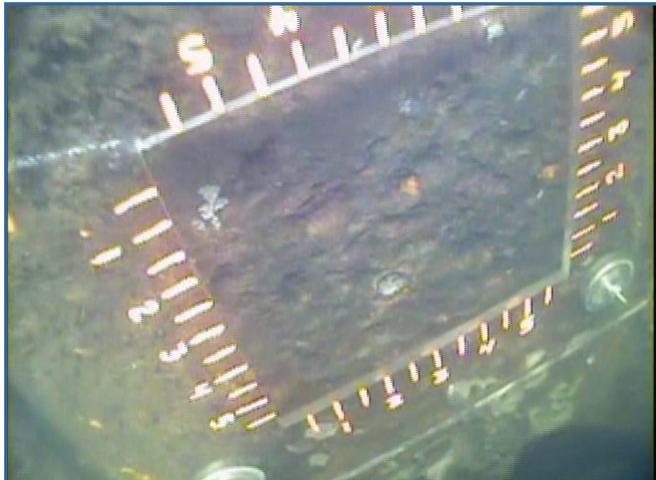


Lakehead Boat Basin (steel sheet pile) - 2 feet

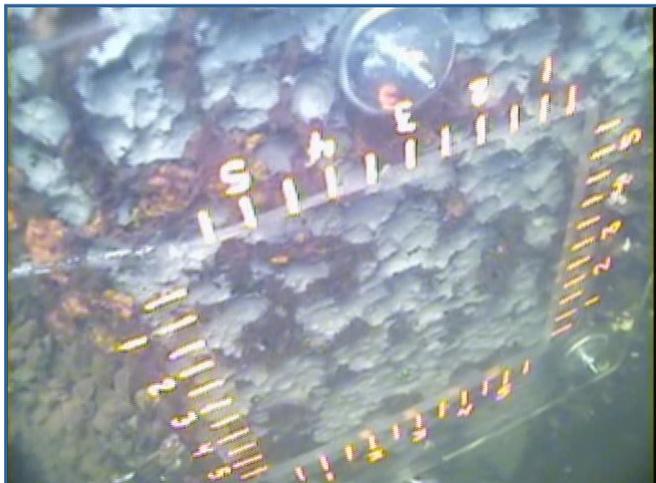


Lakehead Boat Basin (steel sheet pile)- 4 feet

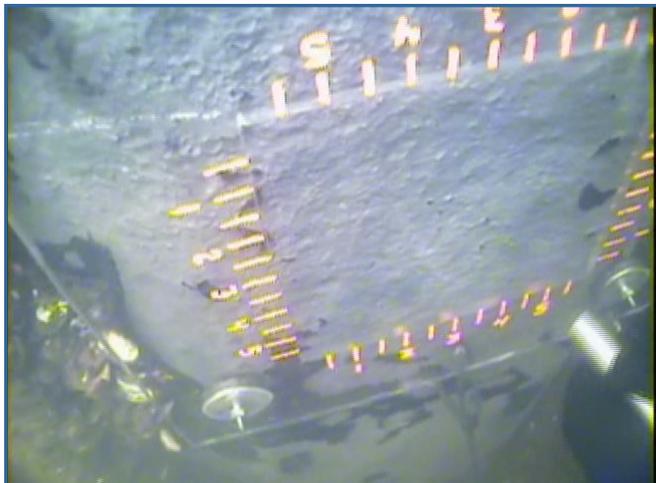




Community Sailing Dock- 0 feet



Community Sailing Dock- 2 feet



Community Sailing Dock- 4 feet





APPENDIX B

Harbor Structure Data Forms

HARBOR STRUCTURES DATA



Site I.D. Number 1

SITE INFORMATION

Facility Duluth Seaway Port Authority

City Duluth Seaway Port Authority

Location Berth 1 Lat./ Long. N46°45.495/ W92°06.151

Facility Information _____

Owner DSPA

STRUCTURE INFORMATION

Wall Length 1600 feet

Depth Driven 58 feet

Average Depth 31 feet

Ice Scour No

Sun Exposure Northwest

Activity Level Moderate

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ38

Era Installed 1950's

Year Installed 1957

Original Thickness Fl=1/2", Wb=3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 2

SITE INFORMATION

Facility Duluth Seaway Port Authority

City Duluth

Location Berth 4 Lat./ Long. N46°45.480/ W92°05.776

Facility Information _____

Owner DSPA

STRUCTURE INFORMATION

Wall Length 2200 feet

Depth Driven 58 feet

Average Depth 31 feet

Ice Scour No

Sun Exposure Northeast

Activity Level High

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ38

Era Installed 1950's

Year Installed 1957

Original Thickness Fl=1/2", Wb=3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 3

SITE INFORMATION

Facility Duluth Seaway Port Authority

City Duluth

Location Berth 6 Lat./ Long. N46°45.495/ W92°06.151

Facility Information _____

Owner DSPA

STRUCTURE INFORMATION

Wall Length 1375 feet

Depth Driven 58 feet

Average Depth 31 feet

Ice Scour No

Sun Exposure Northwest

Activity Level Moderate

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ38

Era Installed 1950's

Year Installed 1957

Original Thickness Fl=1/2", Wb=3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 4

SITE INFORMATION

Facility CN- Two Harbors

City Two Harbors

Location Dock 1 Lat./ Long. N47°00.931/ W91°40.258

Facility Information Taconite Load out Facility

Owner Canadian National Railway

STRUCTURE INFORMATION

Wall Length 1406 feet

Depth Driven unk

Average Depth 30 feet

Ice Scour No

Sun Exposure North

Activity Level Low

Structure Type Bulkhead

Type of Wall Steel Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MP-115

Era Installed 1910's

Year Installed 1912

Original Thickness 0.375

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 5

SITE INFORMATION

Facility Minnesota Slip

City Duluth

Location North Wall Lat./ Long. N46°47.018/ W92°05.865

Facility Information William A. Irvin & Lake Superior and Charter Fishing Docks

Owner Marine Iron & Ship Building Co. and City of Duluth

STRUCTURE INFORMATION

Wall Length 150 feet

Depth Driven unk

Average Depth 16 feet

Ice Scour No

Sun Exposure Southeast

Activity Level Moderate

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ-38

Era Installed unk

Year Installed unk

Original Thickness 1/2"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 6

SITE INFORMATION

Facility DECC

City Duluth

Location DECC Lat./ Long. N46°46.765/ W92°05.906

Facility Information _____

Owner City of Duluth

STRUCTURE INFORMATION

Wall Length 950 Feet

Depth Driven 28 feet

Average Depth 14 Feet

Ice Scour No

Sun Exposure Southeast

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ-38

Era Installed 1964

Year Installed 1960's

Original Thickness Fl=1/2", Wb=3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 7

SITE INFORMATION

Facility Cargill

City Duluth

Location Berth 1 Lat./ Long. N46°46.166/ W92°06.312

Facility Information _____

Owner Cargill Inc.

STRUCTURE INFORMATION

Wall Length 1700 feet

Depth Driven unk

Average Depth 28 feet

Ice Scour No

Sun Exposure Northwest

Activity Level Moderate

Structure Type Bulkhead Wall

Type of Wall Concrete cap w/ timber cribbing, 900 ft fronted w/ sheet pile

PILE INFORMATION

Manufacturer Bethlehem Steel

Type PZ-27

Era Installed unk

Year Installed unk

Original Thickness 3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 8

SITE INFORMATION

Facility Hallett Dock 5

City Duluth

Location North face of Dock 5 Lat./ Long. N46°44.734/ W92°07.943

Facility Information Misc Bulk Material

Owner Hallett Dock Company

STRUCTURE INFORMATION

Wall Length 2400 feet

Depth Driven 50 feet

Average Depth 25 feet

Ice Scour No

Sun Exposure Northeast

Activity Level Moderate

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ-38

Era Installed 1980's

Year Installed 1988

Original Thickness FL=1/2", Wb=3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 9

SITE INFORMATION

Facility Bong Bridge Cell

City Duluth Harbor

Location South side of west pier Lat./ Long. N46°43.882/ W92°08.668

Facility Information _____

Owner Mn/DOT

STRUCTURE INFORMATION

Wall Length _____

Depth Driven _____

Average Depth 27 feet

Ice Scour No

Sun Exposure West

Activity Level Low

Structure Type Pier Protection Cell

Type of Wall Sheet Pile Cell

PILE INFORMATION

Manufacturer US Steel

Type PSA 28

Era Installed 1980's

Year Installed 1986

Original Thickness 1/2"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) Yes

Year Coated 1986

Coating Name unk

Coating Manufacturer unk

Coating Type Coal Tar Epoxy

Location 4 to 8 feet below IGLD

HARBOR STRUCTURES DATA



Site I.D. Number 11

SITE INFORMATION

Facility Spirit Lake Marina

City Duluth

Location Inner Wall Lat./ Long. 46°42.433/ W92°12.172

Facility Information Located on St. Louis River

Owner Jim & Judy King

STRUCTURE INFORMATION

Wall Length 125 feet

Depth Driven _____

Average Depth 8 feet

Ice Scour No

Sun Exposure Southeast

Activity Level Low

Structure Type Wood pile dock

Type of Wall steel jacketed wood piles

PILE INFORMATION

Manufacturer unk

Type 12" Sch 40 Pipe

Era Installed 1980's

Year Installed Late 80's

Original Thickness 0.375

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification _____

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 12

SITE INFORMATION

Facility Oliver Bridge

City Oliver

Location West Pier Lat./ Long. N46°39.391/ W92°12.165

Facility Information Sheet Pile Cell driven around pier to stop scour

Owner Canadian National Railway

STRUCTURE INFORMATION

Wall Length 140 feet

Depth Driven 40 feet

Average Depth 26 feet

Ice Scour no

Sun Exposure South

Activity Level Low

Structure Type Bridge Pier

Type of Wall Sheet Pile Cell

PILE INFORMATION

Manufacturer Bethlehem

Type SP?

Era Installed 1900's

Year Installed unk

Original Thickness .625"

Hot or Cold Rolled Hot

Capped (Yes/No) No

ASTM Specification _____

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 13

SITE INFORMATION

Facility MERC

City Superior

Location Bent 43 Lat./ Long. N46°44.571/ W92°06.891

Facility Information _____

Owner Midwest Energy Resources Co, a Division of Detroit Edison

STRUCTURE INFORMATION

Wall Length 1215 feet

Depth Driven 85

Average Depth 27 feet

Ice Scour No

Sun Exposure Northwest

Activity Level High

Structure Type Steel Pile, Concrete Decked Wharf, Some Steel Jackets

Type of Wall Steel Pile Bents

PILE INFORMATION

Manufacturer UNK

Type HP12x74

Era Installed 1970's

Year Installed 1974

Original Thickness 0.61

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A36

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 14

SITE INFORMATION

Facility CHS

City Superior

Location East Dock Elevator 2 Lat./ Long. N46°44.399/ W92°05.965

Facility Information _____

Owner Cenex Harvest States

STRUCTURE INFORMATION

Wall Length 1175 feet

Depth Driven 50 feet

Average Depth 27

Ice Scour Yes- on concrete

Sun Exposure East

Activity Level Low

Structure Type Conc. Bulkhead supported by timber crib w/ sheet pile front

Type of Wall Steel Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MP115

Era Installed 1960's

Year Installed 1963

Original Thickness 3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Concrete

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 15

SITE INFORMATION

Facility CHS

City Superior

Location West Dock- Inner End Lat./ Long. N46°44.377/ W92°06.155

Facility Information _____

Owner Cenex Harvest States

STRUCTURE INFORMATION

Wall Length 1165 feet

Depth Driven _____

Average Depth 24 feet

Ice Scour Yes- on concrete

Sun Exposure Northwest

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type MZ-27

Era Installed 1960's

Year Installed 1963

Original Thickness 0.375

Hot or Cold Rolled Hot

Capped (Yes/No) Concrete

ASTM Specification _____

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 16

SITE INFORMATION

Facility CHS

City Superior

Location West Dock- Rehab Area Lat./ Long. N46°44.406/ W92°06.151

Facility Information _____

Owner Cenex Harvest States

STRUCTURE INFORMATION

Wall Length 1165 feet

Depth Driven 50 feet

Average Depth 24

Ice Scour No

Sun Exposure Northwest

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer HOESCH

Type 2500

Era Installed 2000

Year Installed 2003

Original Thickness .492FL / .375W

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 17

SITE INFORMATION

Facility Cutler Magner
 City Superior
 Location North Wall Lat./ Long. N46°43.993/ W92°04.498
 Facility Information Limestone Dock
 Owner Cutler Magner Co

STRUCTURE INFORMATION

Wall Length 570 feet
 Depth Driven 55 feet
 Average Depth 24 feet
 Ice Scour No
 Sun Exposure Northwest
 Activity Level Moderate
 Structure Type Bulkhead Wall
 Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel
 Type MZ-32
 Era Installed 1960's
 Year Installed _____
 Original Thickness Fl= 1/2", Wb=3/8"
 Hot or Cold Rolled Hot
 Capped (Yes/No) Yes
 ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No
 Year Coated _____
 Coating Name _____
 Coating Manufacturer _____
 Coating Type _____
 Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 18

SITE INFORMATION

Facility Lakehead Boat Basin

City Duluth

Location North Pier Lat./ Long. N46°46.457/ W92°05.563

Facility Information Private boat marina

Owner Joel Johnson

STRUCTURE INFORMATION

Wall Length 250 feet

Depth Driven 20 feet

Average Depth 8 feet

Ice Scour No

Sun Exposure Northwest

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type PZ-27

Era Installed 2000

Year Installed 2002

Original Thickness 0.375

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) Yes

Year Coated 2002

Coating Name Galvanizing

Coating Manufacturer

Coating Type Hot Dip Galvanized

Location Full Length

HARBOR STRUCTURES DATA



Site I.D. Number 19

SITE INFORMATION

Facility Lakehead Boat Basin

City Duluth

Location South Wall Lat./ Long. N46°46.454/ W92°05.522

Facility Information Private boat marina

Owner Joel Johnson

STRUCTURE INFORMATION

Wall Length 175 feet

Depth Driven 12 feet

Average Depth 5 feet

Ice Scour No

Sun Exposure Northwest

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type PSA 23

Era Installed 1960's

Year Installed 1965

Original Thickness 3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

HARBOR STRUCTURES DATA



Site I.D. Number 20

SITE INFORMATION

Facility Community Sailing Dock

City Duluth

Location Outer Wall Lat./ Long. N46°43.932/ W92°03.408

Facility Information Operated by Duluth Community Sailing Assoc.

Owner City of Duluth

STRUCTURE INFORMATION

Wall Length 50 feet

Depth Driven unk

Average Depth 5 feet

Ice Scour No

Sun Exposure Southwest

Activity Level Low

Structure Type Bulkhead Wall

Type of Wall Anchored Sheet Pile

PILE INFORMATION

Manufacturer US Steel

Type PMA 22

Era Installed unk

Year Installed unk

Original Thickness 3/8"

Hot or Cold Rolled Hot

Capped (Yes/No) Yes

ASTM Specification A328

COATING INFORMATION

Coating (Y/N) No

Year Coated _____

Coating Name _____

Coating Manufacturer _____

Coating Type _____

Location _____

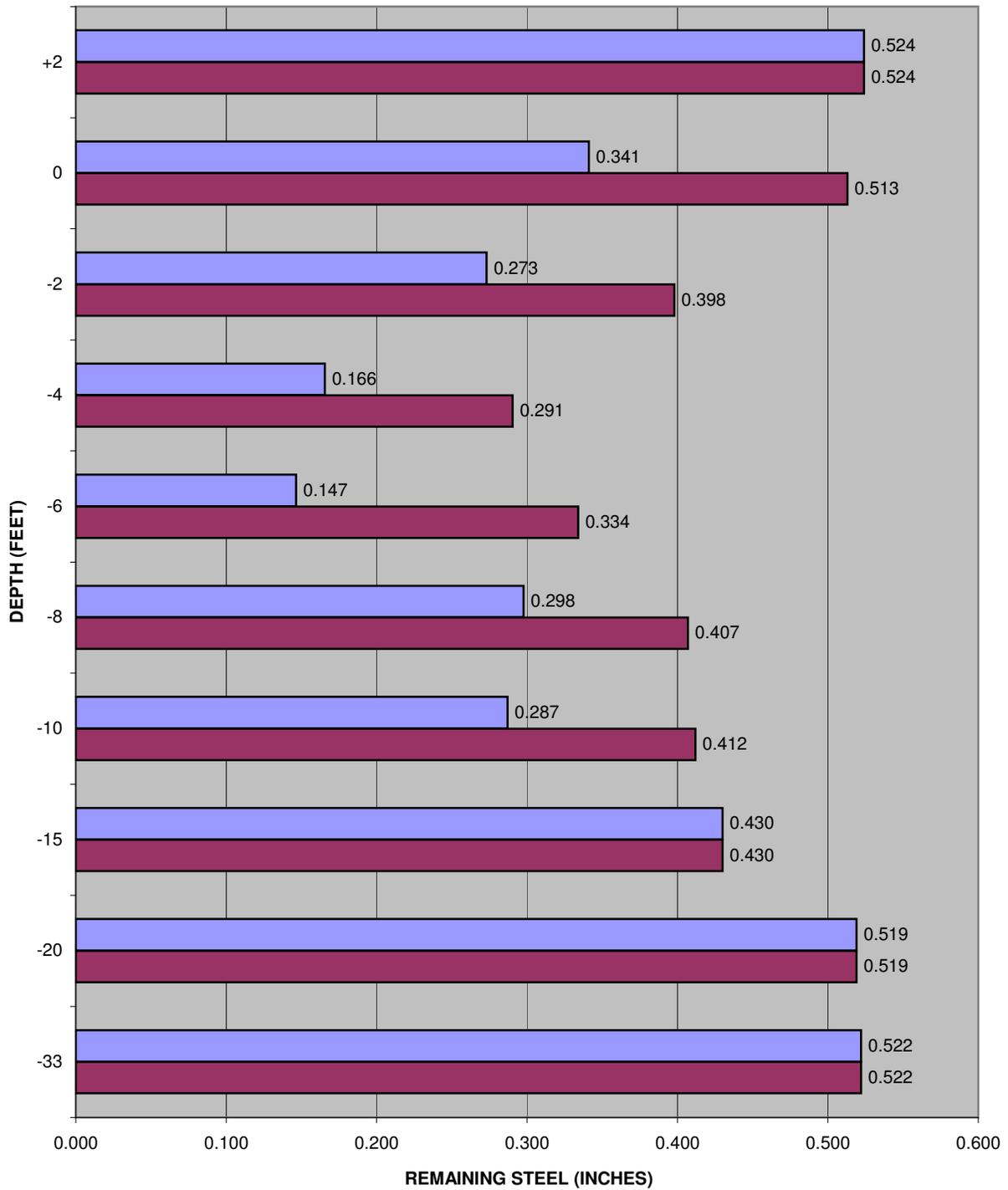


APPENDIX C

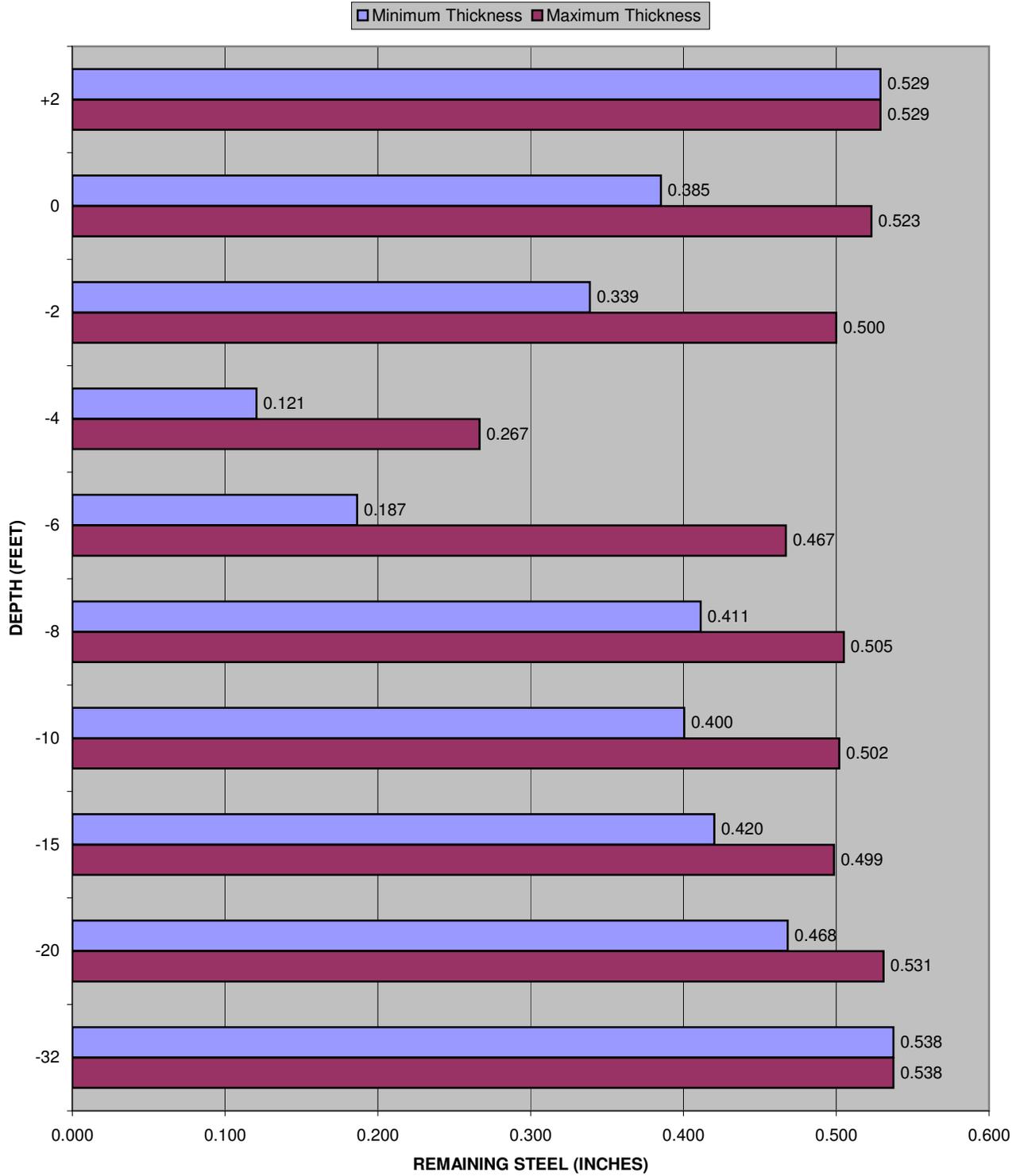
Corrosion Data Forms

DSPA BERTH 1 - REMAINING STEEL
SITE I.D. # 1
(Measured Steel Thickness of 0.524 inches)

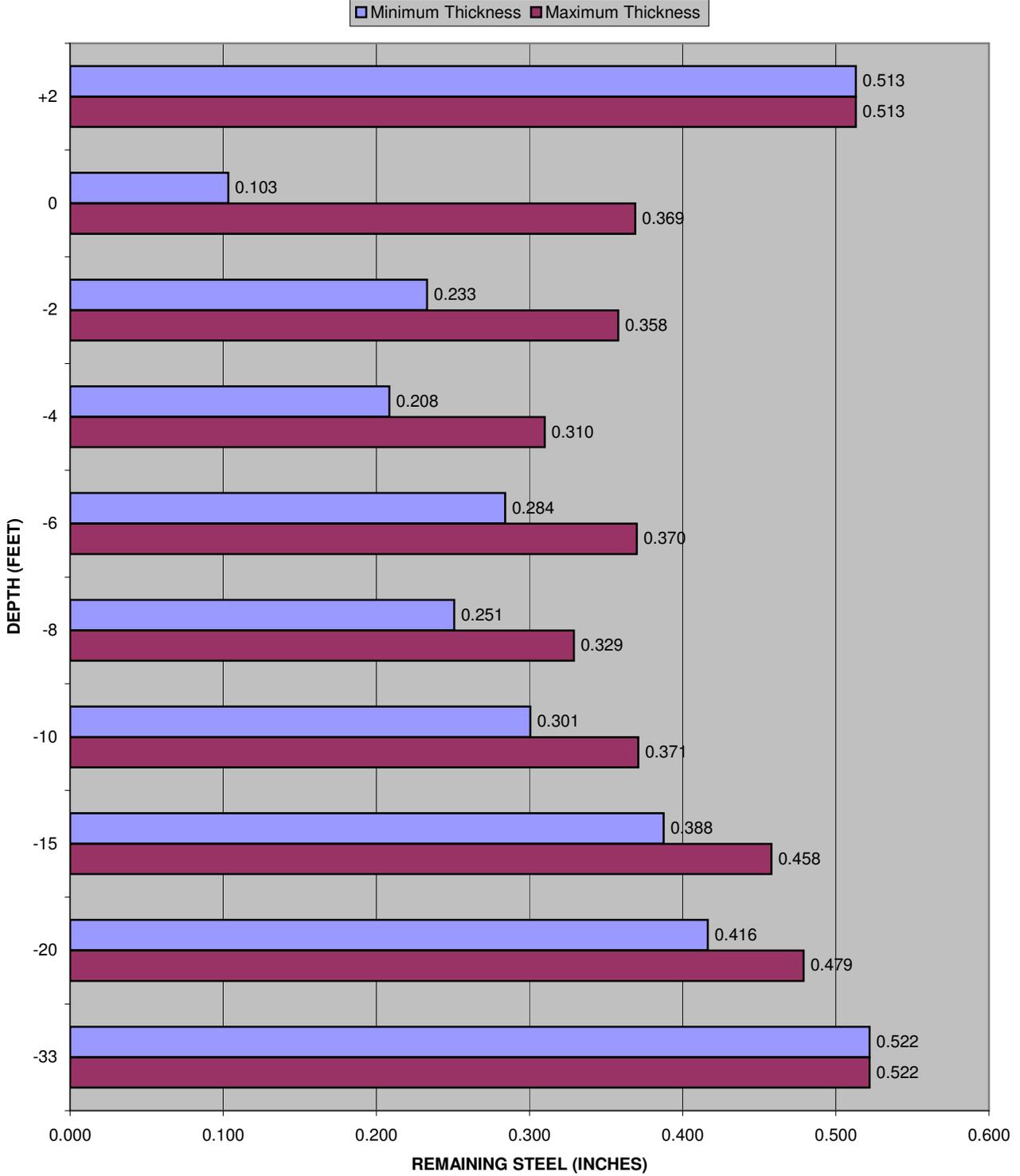
Minimum Thickness Maximum Thickness



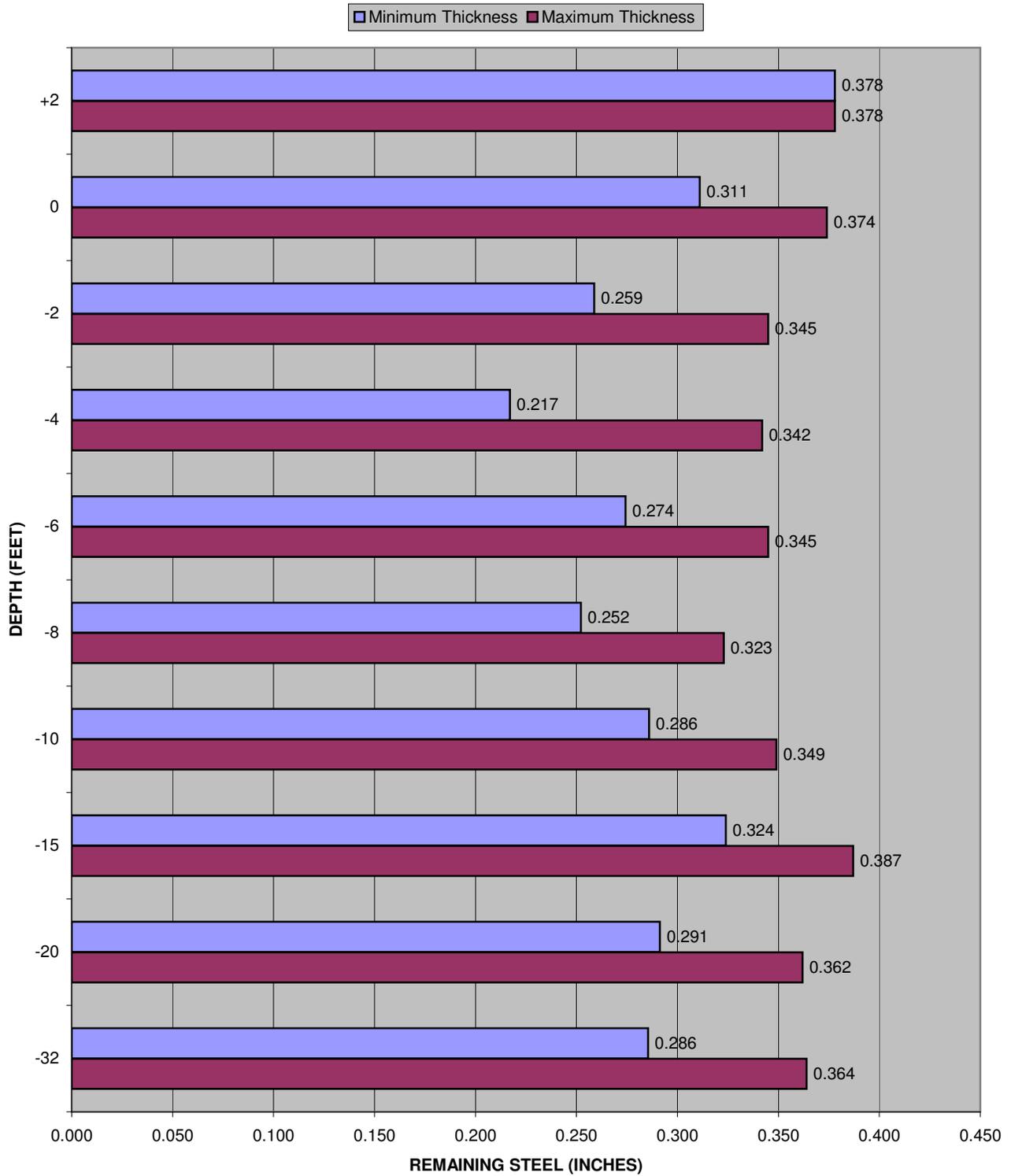
DSPA BERTH 4- REMAINING STEEL
SITE I.D. # 2
(Measured Steel Thickness of 0.529)



DSPA BERTH 6- REMAINING STEEL
SITE I.D. # 3
(Measured Steel Thickness of 0.522 inches)



CN TWO HARBORS- REMAINING STEEL
SITE I.D. # 4
(Measured Steel Thickness of 0.378 inches)

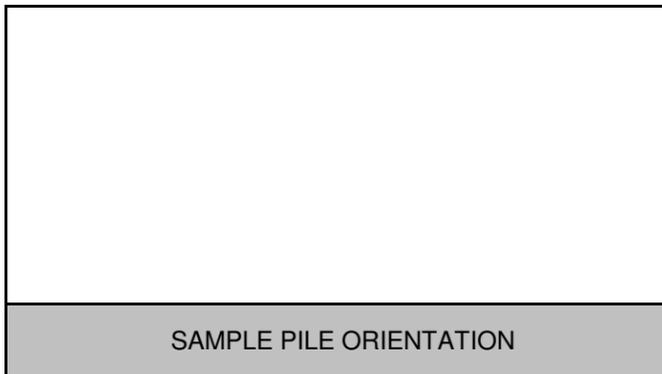


HARBOR STRUCTURES DATA



FACILITY Minnesota Slip
 DOCK CONFIGURATION Southwest- Northeast
 EXPOSURE DIRECTION Southeast

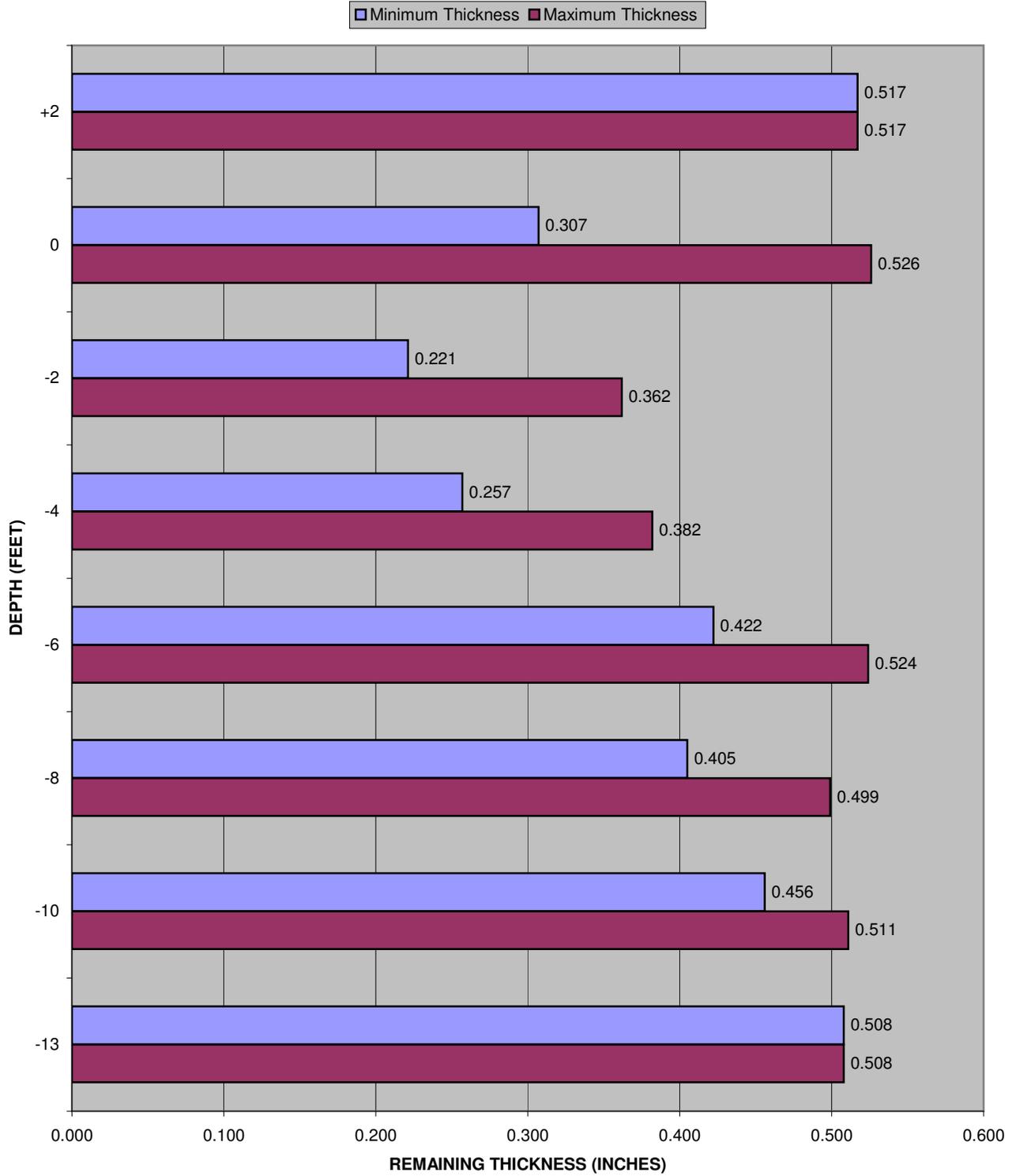
SITE I.D. NUMBER 5
 INSPECTION DATE 8/2/2006
 INSPECTION TIME 11:10
 WATER ELEVATION 601.7
 TEAM LEADER Chad Scott



SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	MZ 38	0.5"	unk

STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments			
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings								
														1	2	3	4	AVG	1	2	3	4	AVG				
1	+2												0.517													Storm sewer outfall by sample point	
2	0	x	White Coating	0.125	100%					x	Pit	Mod	0.526	0.125	0.250	0.188	0.313	0.219	0.500	0.750	0.625	0.625	0.625				
3	-2	x	orange nod / Algae	.25 to .75	75%					x	Pit	Mod	0.362	0.125	0.125	0.125	0.188	0.141	0.375	0.500	0.500	0.500	0.469			Orange Nodules- Larger & Softer	
4	-4	x	orange nod / Algae	.25 to .75	75%					x	Pit	Mod	0.382	0.094	0.125	0.125	0.156	0.125	0.125	0.250	0.250	0.250	0.250	0.219			Less Pitting on in Pan
5	-6	x	Mussels/ sponges	.5 to .75	75% 25%					x	Pit	Low	0.524	0.063	0.094	0.125	0.125	0.102	0.250	0.125	0.250	0.575	0.300			Sporadic Pitting	
6	-8	x	Mussels/ sponges/O Nod	.5 to .75	70/20/10					x	Pit	Low	0.499	0.094	0.094	0.125	0.063	0.094	0.250	0.250	0.188	0.125	0.203			Etched surface / small pits	
7	-10	x	Orange Nod - Z mussels	.5 to .75	50% 50%					x	Uniform	Low	0.511	0.063	0.063	0.031	0.063	0.055	0.125	0.125	0.063	0.125	0.110			Etched surface / small pits	
8	-13	x	Orange Nod - Z mussels	.5 to .75	50% 50%								0.508					0.000						0.000		Mudline @13 ft, Soft Silty bottom / smooth steel	
9	-20																	0.000						0.000			
10	ML																	0.000						0.000			

MINNESOTA SLIP- REMAINING STEEL
SITE I.D. # 5
(Measured Steel Thickness of 0.517 inches)

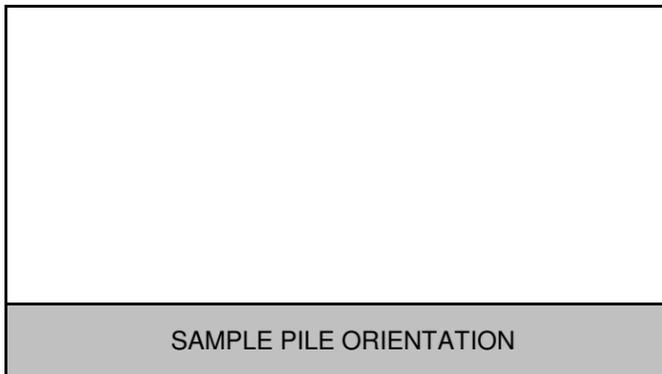


HARBOR STRUCTURES DATA



FACILITY _____ DECC _____
 DOCK CONFIGURATION _____ Southwest- Northeast _____
 EXPOSURE DIRECTION _____ Southeast _____

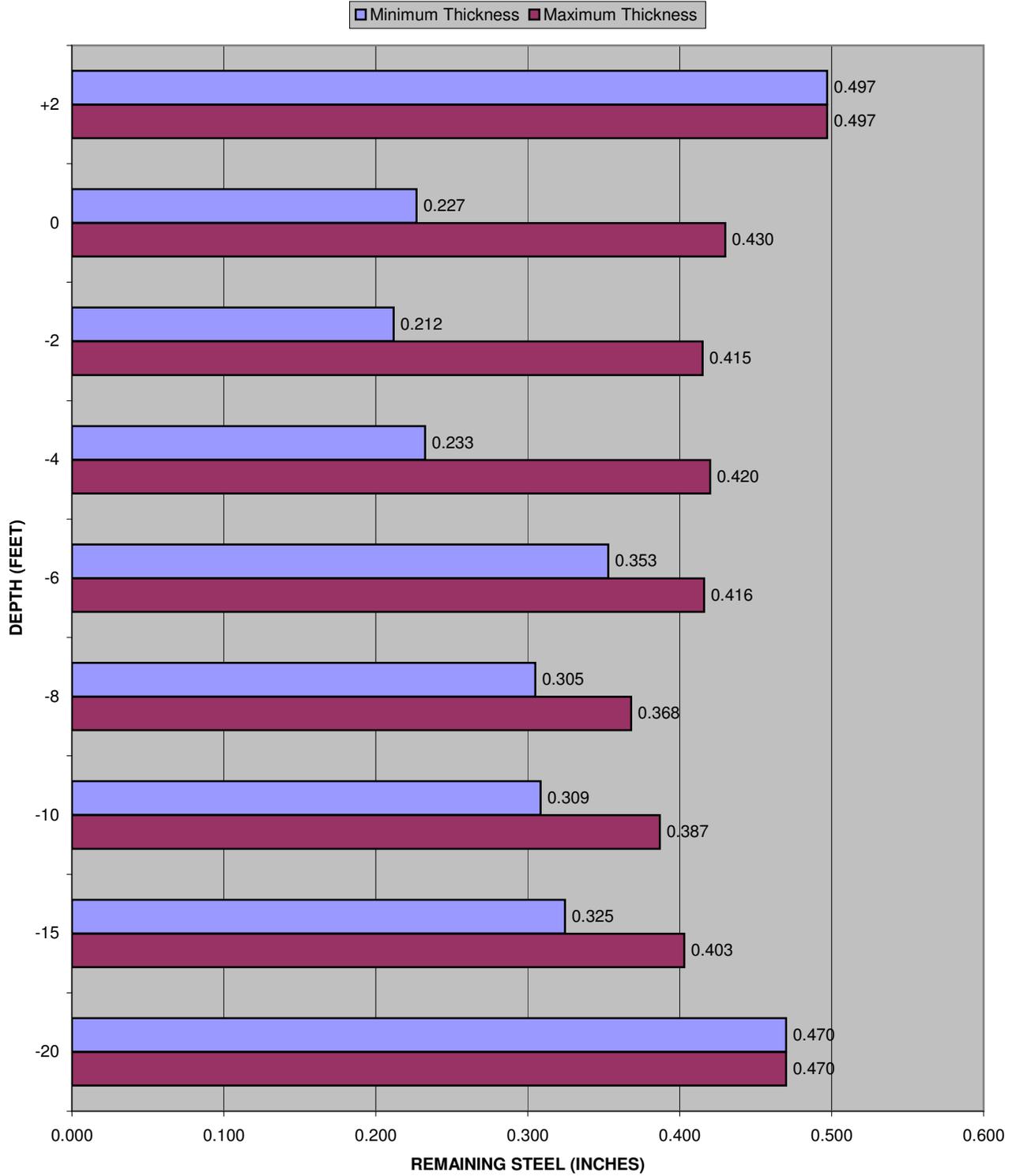
SITE I.D. NUMBER _____ 6 _____
 INSPECTION DATE _____ 8/2/2006 _____
 INSPECTION TIME _____ 9:20 _____
 WATER ELEVATION _____ 601.71 _____
 TEAM LEADER _____ Chad Scott _____



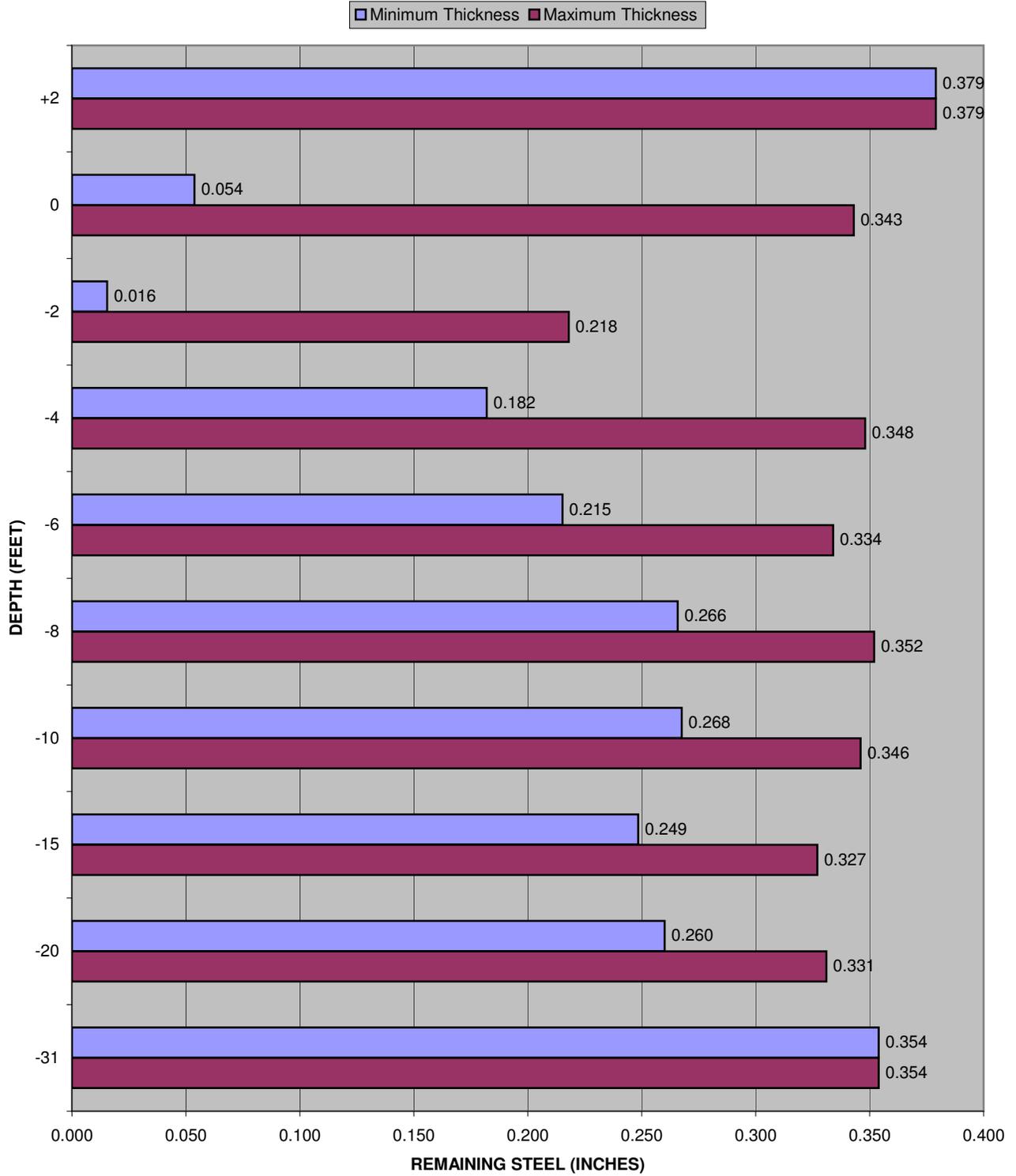
SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	MZ 38	0.5"	1964

STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments	
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings						
														1	2	3	4	AVG	1	2	3	4	AVG		
1	+2					x	Coal / Tar	unk	unk				0.497												Present Above IGLD
2	0	x	Algae/orange nod / white	<.25	100%					x	Pit	High	0.430	0.125	0.250	0.188	0.250	0.203	0.500	0.750	0.500	0.750	0.625		Heavy Pits on both out & in pans
3	-2	x	Algae/ Mussels	.25 to 1.0	Sporadic					x	Pit	High	0.415	0.188	0.250	0.125	0.250	0.203	0.500	0.750	0.500	0.625	0.594		small pits within large pits
4	-4	x	Algae/mussels/s porges	.25 to 1.0	Sporadic					x	Pit	High	0.420	0.125	0.250	0.125	0.250	0.188	0.500	0.500	0.500	0.500	0.500		less pitting on in pans
5	-6	x	Algae/mussels/s porges	.25 to 1.0	Sporadic					x	Pit	Mod	0.416	0.063	0.063	0.063	0.063	0.063	0.188	0.250	0.250	0.125	0.203		pits on in &out pans similar
6	-8	x	Algae/mussels/s porges	.25 to 1.0	Sporadic					x	Pit	Mod	0.368	0.063	0.063	0.063	0.063	0.063	0.250	0.125	0.250	0.188	0.203		pits on in &out pans similar
7	-10	x	Less Algae more Mussels	1 to 1.5	80% 20%					x	Pit	Mod	0.387	0.063	0.063	0.094	0.094	0.079	0.188	0.125	0.188	0.250	0.188		pits on in &out pans similar
8	-15	x	Mussels	1 to 1.5	100%					x	Uniform	Low	0.403	0.094	0.063	0.000	0.000	0.079	0.500	0.250	0.000	0.000	0.375		Only 2 pits in sample area
9	-20	x	Mussels	1 to 1.5	100%					x	Uniform	Low	0.470					0.000					0.000		Etched surface / Mud line @ 20 ft
10	ML																								

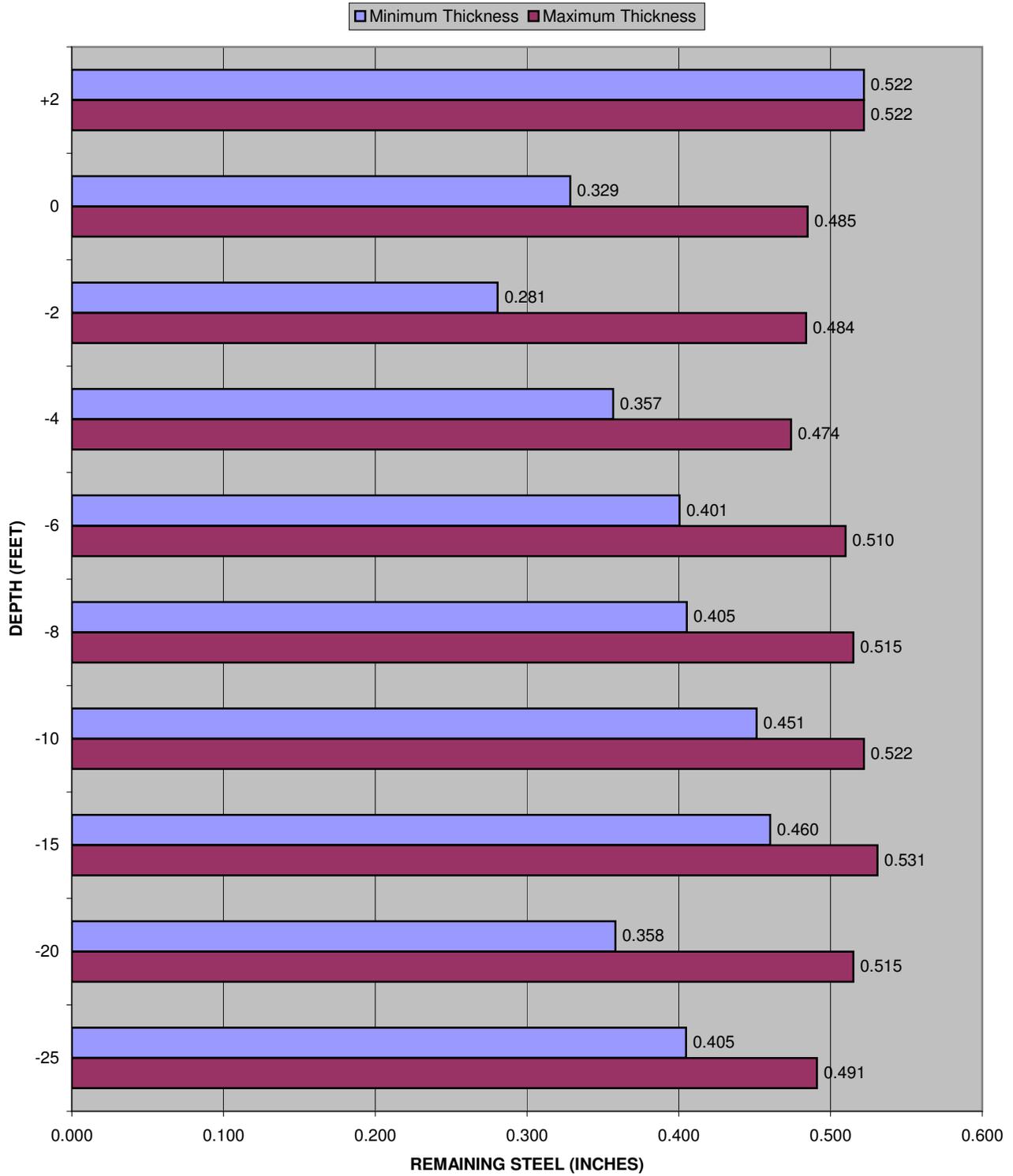
DECC DOCK- REMAINING STEEL
SITE I.D. # 6
(Measured Steel Thickness of 0.497 inches)



CARGILL DOCK- REMAINING STEEL
SITE I.D. # 7
(Measured Steel Thickness of 0.379 inches)



HALLETT DOCK 5- REMAINING steel
SITE I.D. # 8
(Measured Steel Thickness of 0.524 inches)

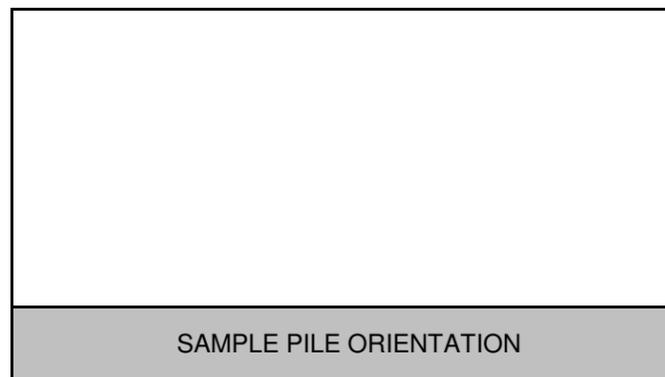


HARBOR STRUCTURES DATA



FACILITY Bong Bridge Cell
 DOCK CONFIGURATION Circular Cell
 EXPOSURE DIRECTION South

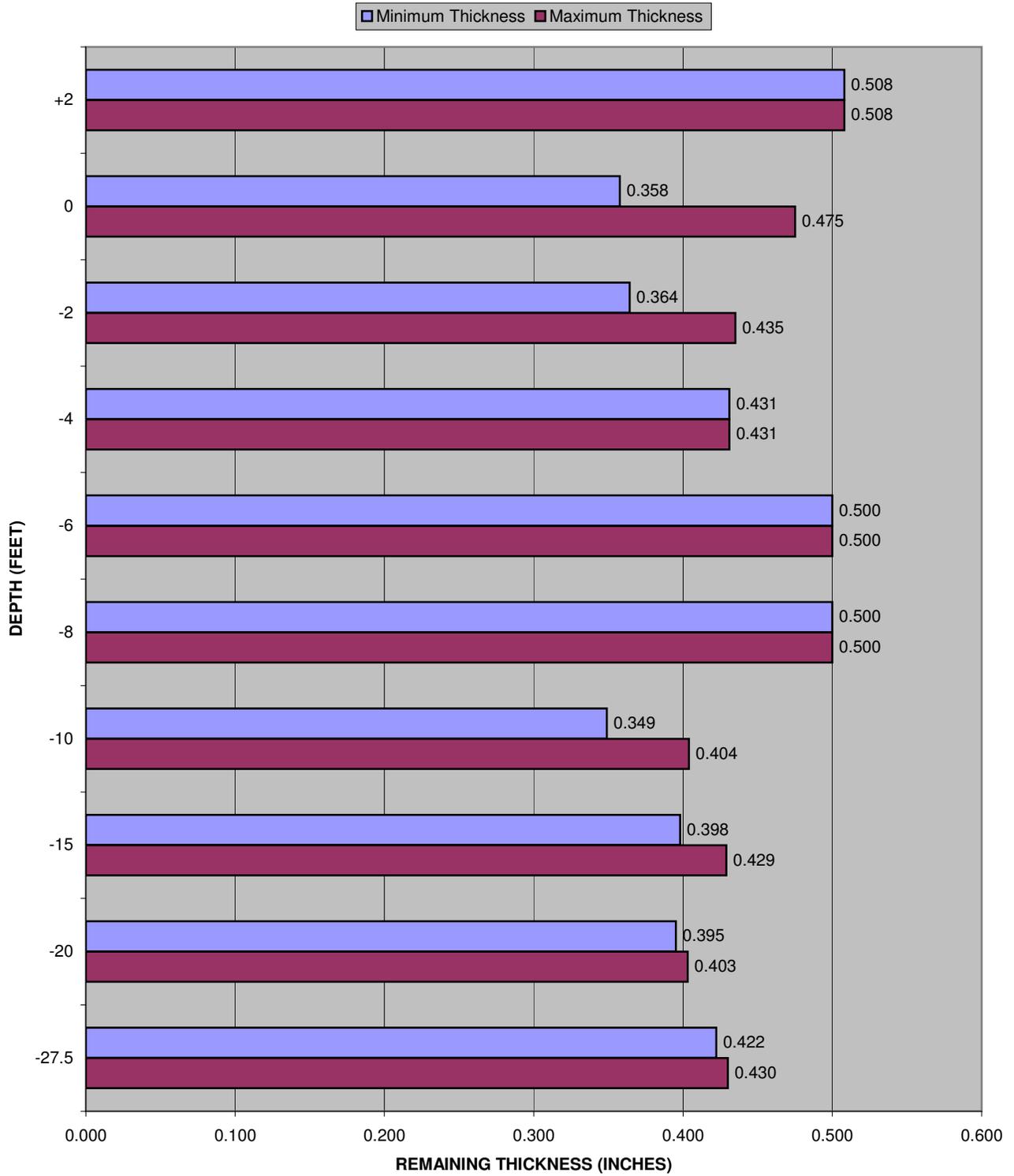
SITE I.D. NUMBER 9
 INSPECTION DATE 8/1/2006
 INSPECTION TIME 8:15
 WATER ELEVATION 601.81
 TEAM LEADER Chad Scott



SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	PSA 28	0.5"	1980's

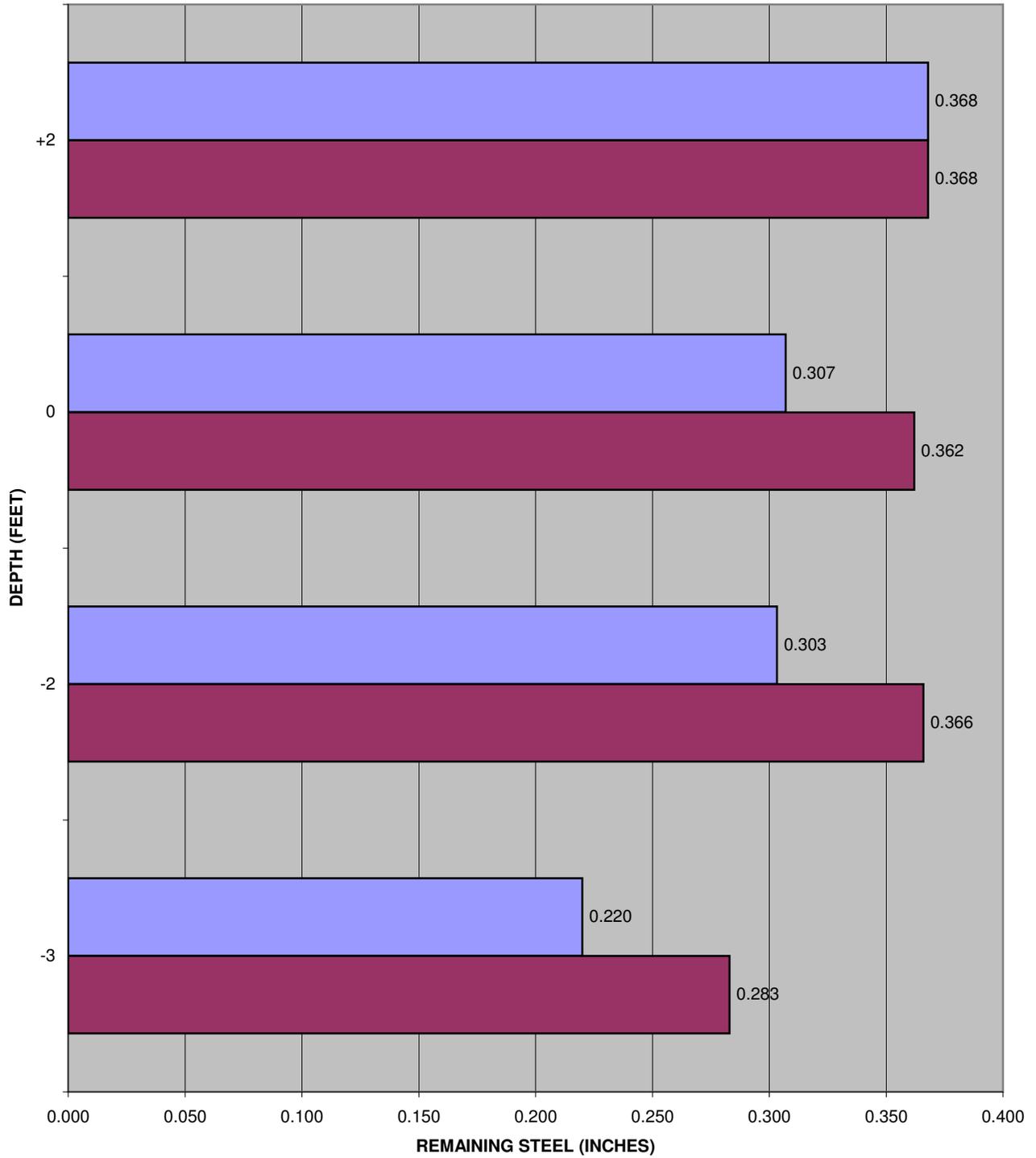
STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments			
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings								
														1	2	3	4	AVG	1	2	3	4	AVG				
1	+2					x	Coal - Tar	unk	100%				0.508														
2	0	x	slime	<.25						x	Pitting	Mod	0.475	0.125	0.063	0.156	0.125	0.117	0.500	0.500	0.500	0.750	0.563		start pitting @ 0ft, coating gone below igld		
3	-2	x	mussels	.5 to .75	sporadic					x	Pitting	High	0.435	0.063	0.094	0.063	0.063	0.071	0.250	0.375	0.125	0.250	0.250		high concentration of small pits		
4	-4	x	mussels	.5 to .75	sporadic	x	Coal - Tar	unk	50%				0.431					0.000						0.000	did not remove coating		
5	-6	x	mussels, sponges	.75 to 1.5	100%	x	Coal - Tar	unk	100%				0.500					0.000						0.000	did not remove coating		
6	-8	x	mussels	1.5 to 2	100%	x	Coal - Tar	unk	100%				0.500					0.000						0.000	coating ends		
7	-10	x	mussels, sponges	1.5 to 2	100%					x	Pitting	High	0.404	0.031	0.063	0.063	0.063	0.055	0.125	0.125	0.125	0.063	0.110		steel in good condition, etched surface		
8	-15	x	mussels	1.5 to 2	100%					x		High	0.429	0.031	0.031	0.031	0.031	0.031	0.500	0.375	0.750	0.750	0.594		ring pattern pits , etched surface		
9	-20	x	mussels	1.5 to 2	100%					x		Mod	0.403	0.031				0.008	0.500	0.375	0.500	0.500	0.469		ring pattern pits, etched surface		
10	-27.5	x	mussels	1.5 to 2	100%					x		Mod	0.430	0.031				0.008	0.250	0.125	0.250	0.125	0.188		27.5 feet deep, minor pitting, etched surface		

BONG BRIDGE CELL- REMAINING STEEL
SITE I.D. # 9
(Measured Steel Thickness of 0.508 inches)

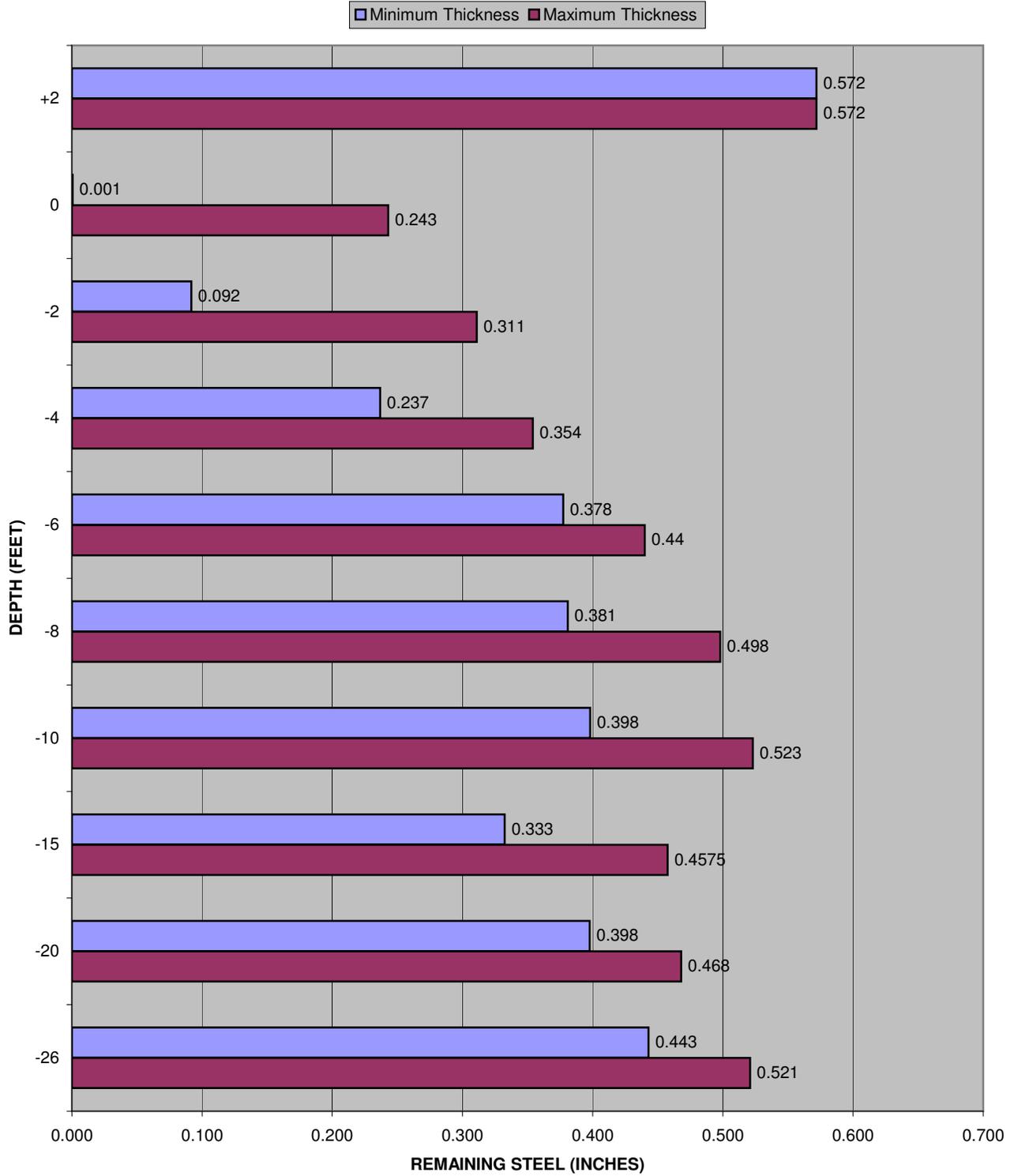


SPIRIT LAKE MARINA- REMAINING STEEL
SITE I.D. # 11
(Measured Steel Thickness of 0.368 inches)

Minimum Thickness Maximum Thickness



OLIVER BRIDGE- REMAINING STEEL
SITE I.D. # 12
(Measured Steel Thickness of 0.572 inches)

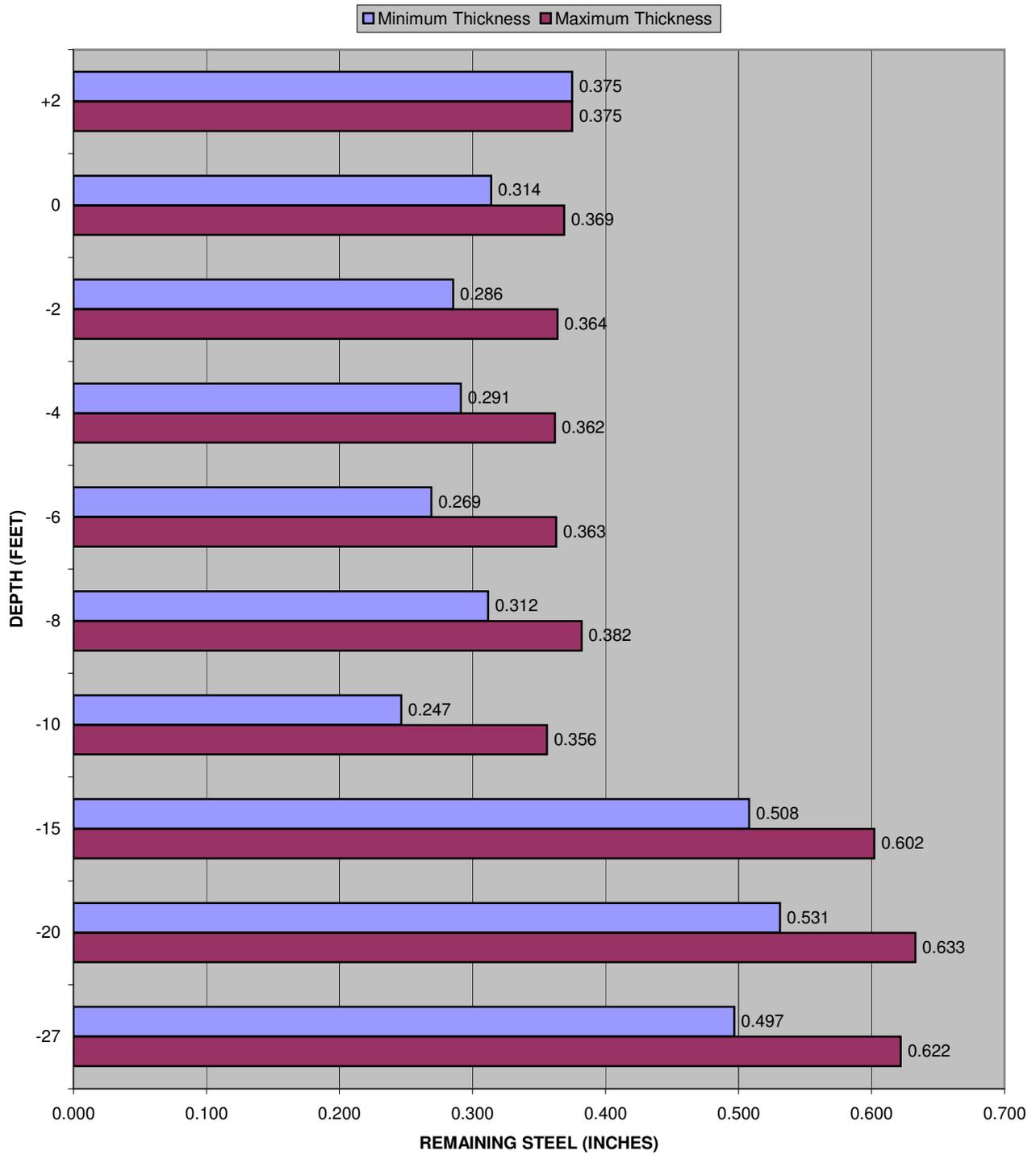


MIDWEST ENERGY 1- REMAINING STEEL

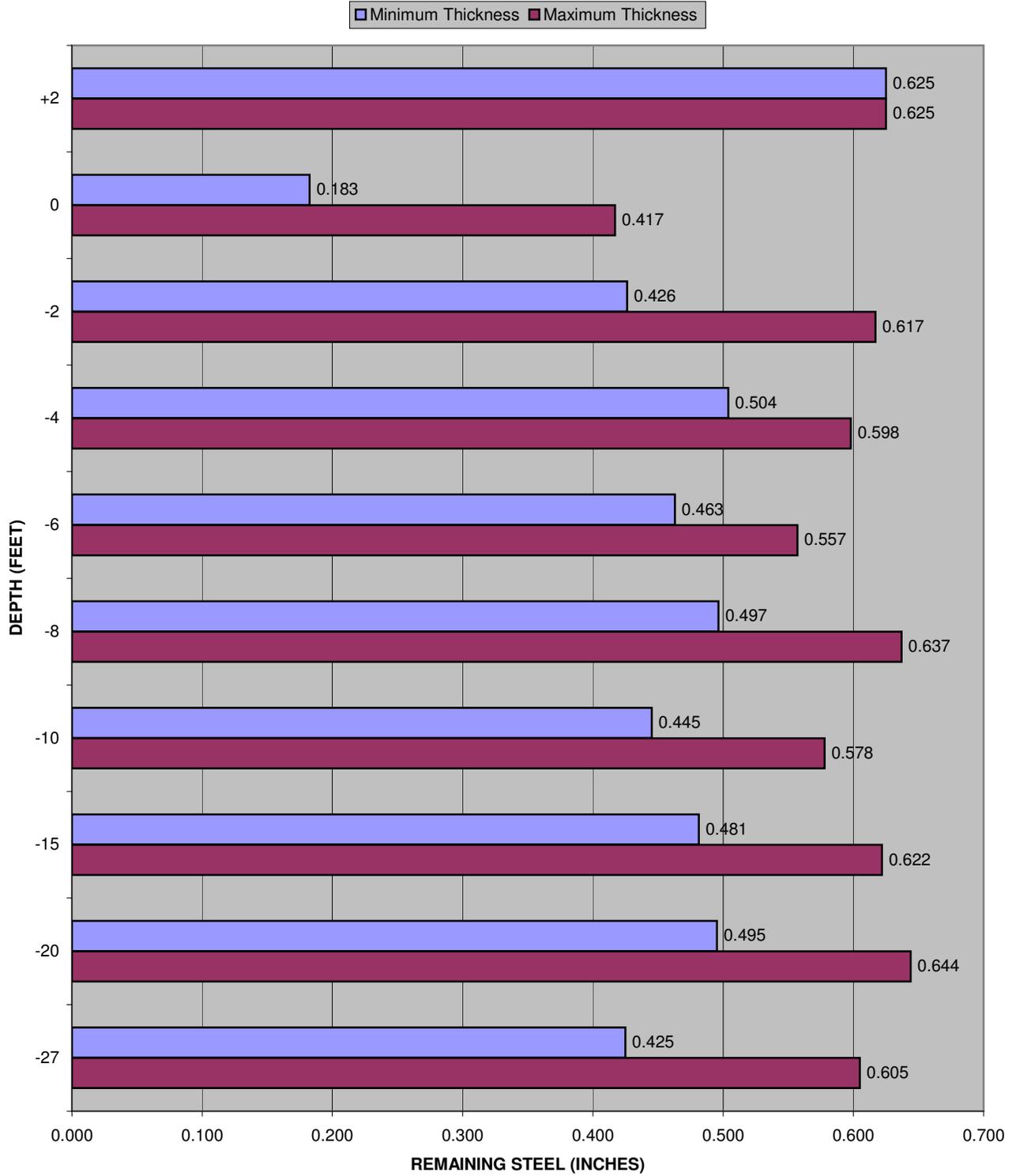
SITE I.D. # 13A

(Measured Jacket Steel Thickness of 0.375 inches, +2 ft to -6 ft)

(Measured H-Pile Steel Thickness of 0.622 inches, -8 ft to -27 ft)



MIDWEST ENERGY 2- REMAINING STEEL
SITE I.D. # 13B
(Measured H-Pile Flange Steel Thickness of 0.625 inches)

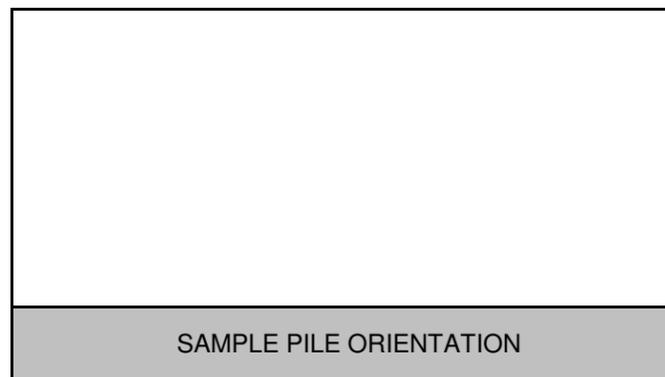


HARBOR STRUCTURES DATA



FACILITY Cenex Harvest States Loc #1
 DOCK CONFIGURATION North- South
 EXPOSURE DIRECTION East

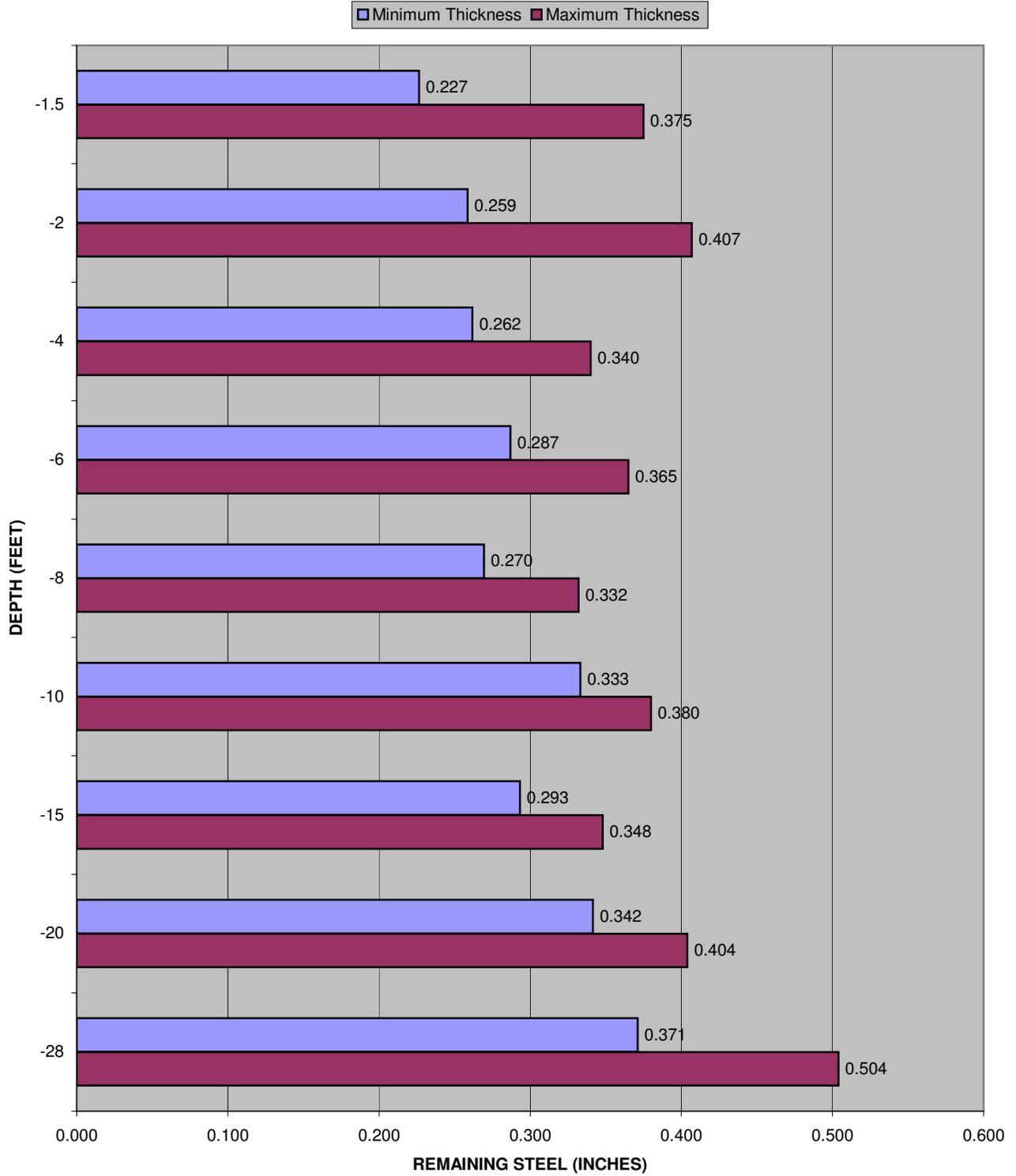
SITE I.D. NUMBER 14
 INSPECTION DATE 8/8/2006
 INSPECTION TIME 12:00
 WATER ELEVATION 601.6
 TEAM LEADER Chad Scott



SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	MP 116	0.375"	1963

STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings					
														1	2	3	4	AVG	1	2	3	4	AVG	
1	+2																						Concrete Cap IglD To -1.5ft	
2	-1.5	x	ON, AL	.25 to .5	75-100					X	Pitting	High	0.375	0.125	0.125	0.156	0.188	0.148	0.625	0.750	0.625	0.750	0.688	Concrete Cap IglD To -1.5ft
3	-2	x	ON, AL	.25 to .5	75-100					X	Pitting	High	0.407	0.125	0.125	0.156	0.188	0.148	0.625	0.750	0.625	0.750	0.688	IP-OP SAME PIT
4	-4	x	ON, ZM, AL	.25 to .5	75-100					X	Pitting	High	0.340	0.125	0.063	0.063	0.063	0.078	0.500	0.500	0.500	0.375	0.469	IP SMALLER, OP LARGER PIT
5	-6	x	ON, ZM, AL	.25 to 1.5	75-100					X	Pitting	High	0.365	0.125	0.063	0.063	0.063	0.078	0.500	0.250	0.250	0.250	0.313	IP SMALLER, OP LARGER PIT
6	-8	x	ON, ZM, AL	.25 to 1.5	75-100					X	Pitting	High	0.332	0.063	0.063	0.063	0.063	0.063	0.250	0.250	0.188	0.250	0.234	IP SAME AS OP
7	-10	x	ON, ZM, AL	.25 to 1.5	50-50					X	Pitting	High	0.380	0.031	0.063	0.063	0.031	0.047	0.188	0.125	0.250	0.188	0.188	OP HIGHER PIT
8	-15	x	ON, ZM, AL	.25 to 1.5	50-50					X	Pitting	High	0.348	0.031	0.063	0.063	0.063	0.055	0.125	0.125	0.188	0.125	0.141	IP SAME AS OP
9	-20	x	ON, ZM, AL	.25 to 1.5	50-50					X	Pitting	Mod	0.404	0.063	0.063	0.063	0.063	0.063	0.250	0.250	0.125	0.125	0.188	IP SAME AS OP
10	-28	x	ON	.25 to .5	100-75					X	Pitting	Low	0.504	0.063	0.156	0.156	0.156	0.133	0.250	0.375	0.125	0.125	0.219	1' LIGHT SILT- IP SAME At ML AS OP

CENEX/ HARVEST STATES #1- REMAINING STEEL
SITE I.D. # 14
(Measured Steel Thickness of 0.504 inches)

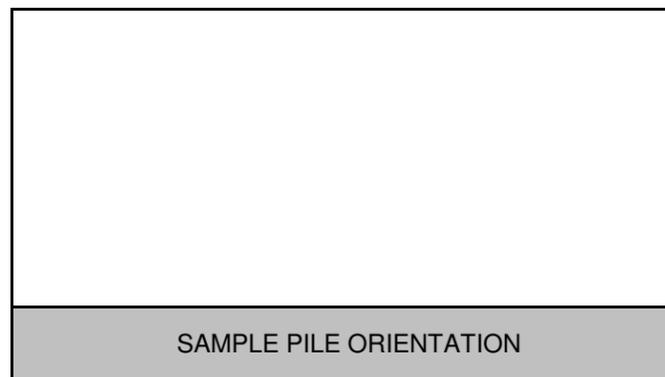


HARBOR STRUCTURES DATA



FACILITY Cenex Harvest States Loc #2
 DOCK CONFIGURATION Southwest- Northeast
 EXPOSURE DIRECTION Northwest

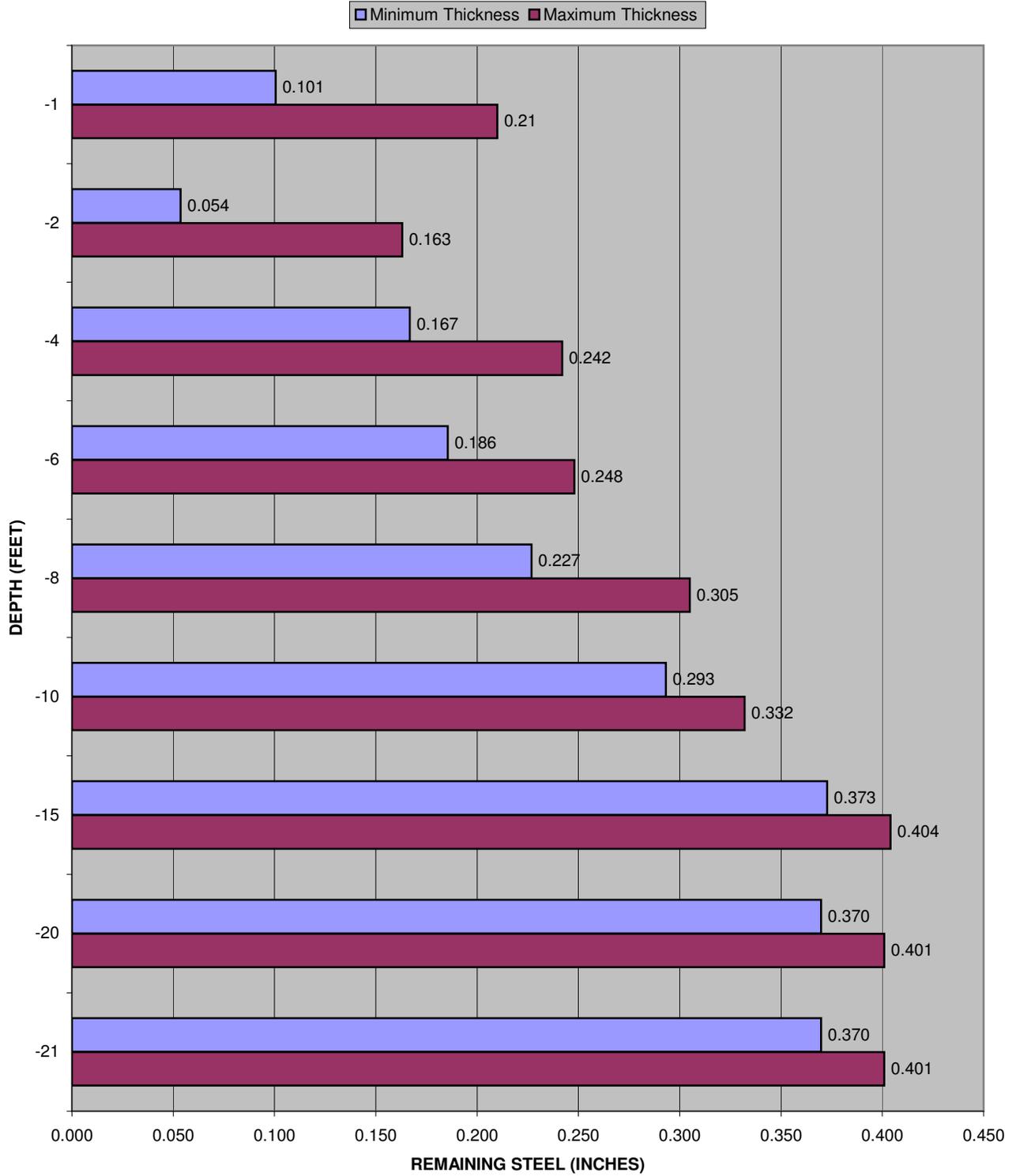
SITE I.D. NUMBER 15
 INSPECTION DATE 8/8/2006
 INSPECTION TIME 14:30
 WATER ELEVATION 601.85
 TEAM LEADER Chad Scott



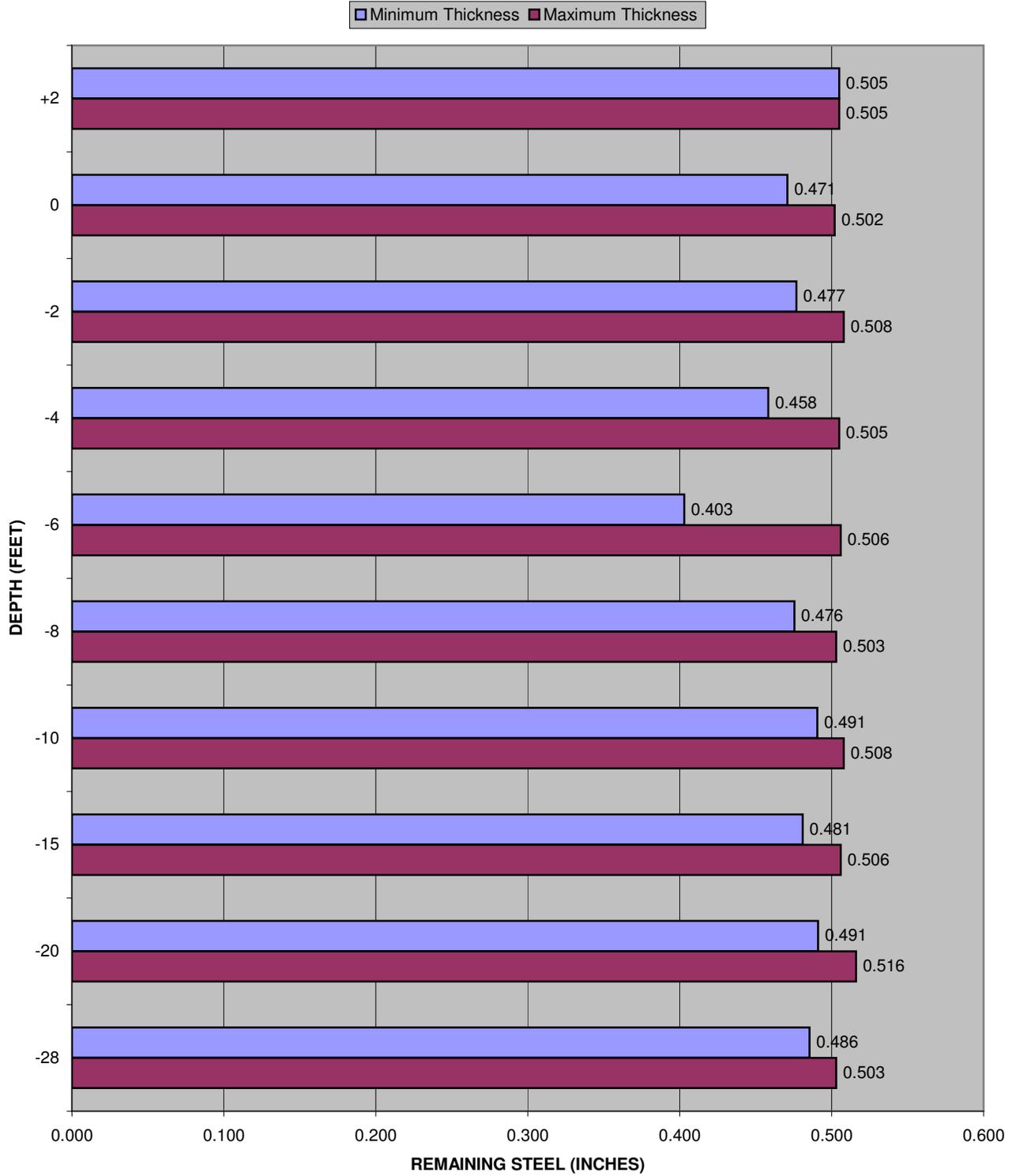
SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	MP 116	0.375"	1957

STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings					
														1	2	3	4	AVG	1	2	3	4	AVG	
1	+2																						Concrete Cap	
2	-1	X	ZM	1	100%					x	Pitting	High	0.21	0.125	0.125	0.125	0.063	0.109	0.375	0.250	0.250	0.375	0.313	Sheets Start 1ft Below IGLD
3	-2	X	ZM	1	100%					x	Pitting	High	0.163	0.125	0.125	0.125	0.063	0.109	0.375	0.250	0.250	0.375	0.313	IP of Same
4	-4	X	ZM, SP	1.5	100%					x	Pitting	High	0.242	0.063	0.082	0.094	0.063	0.075	0.250	0.500	0.500	0.375	0.406	IP OP Same
5	-6	X	ZM	1.5	100%					x	Pitting	High	0.248	0.063	0.063	0.063	0.063	0.063	0.250	0.250	0.250	0.250	0.250	IP OP Same
6	-8	X	ZM, SP	1.5	100%					x	Pitting	High	0.305	0.063	0.094	0.063	0.094	0.078	0.250	0.375	0.375	0.500	0.375	OP Heavy Pit thru IP
7	-10	X	ZM, SP	1.5	100%					x	Pitting	High	0.332	0.031	0.031	0.063	0.031	0.039	0.250	0.375	0.250	0.375	0.313	IP same as OP
8	-15	X	ZM	1.5	100%					x	Pitting	High	0.444	0.031	0.031	0.031	0.031	0.031	0.188	0.063	0.188	0.375	0.203	IP same as OP
9	-20	X	ZM	1.5	50%					x	Pitting	Low	0.401	0.031	0.031	0.031	0.031	0.031	0.188	0.063	0.188	0.063	0.125	IP same as OP
10	-21	X	ZM	1.5	50%					x	Pitting	Low	0.401	0.031	0.031	0.031	0.031	0.031	0.188	0.063	0.188	0.063	0.125	IP same as OP

CENEX/ HARVEST STATES #2- REMAINING STEEL
SITE I.D. # 15
(Measured Steel Thickness of 0.404 inches)

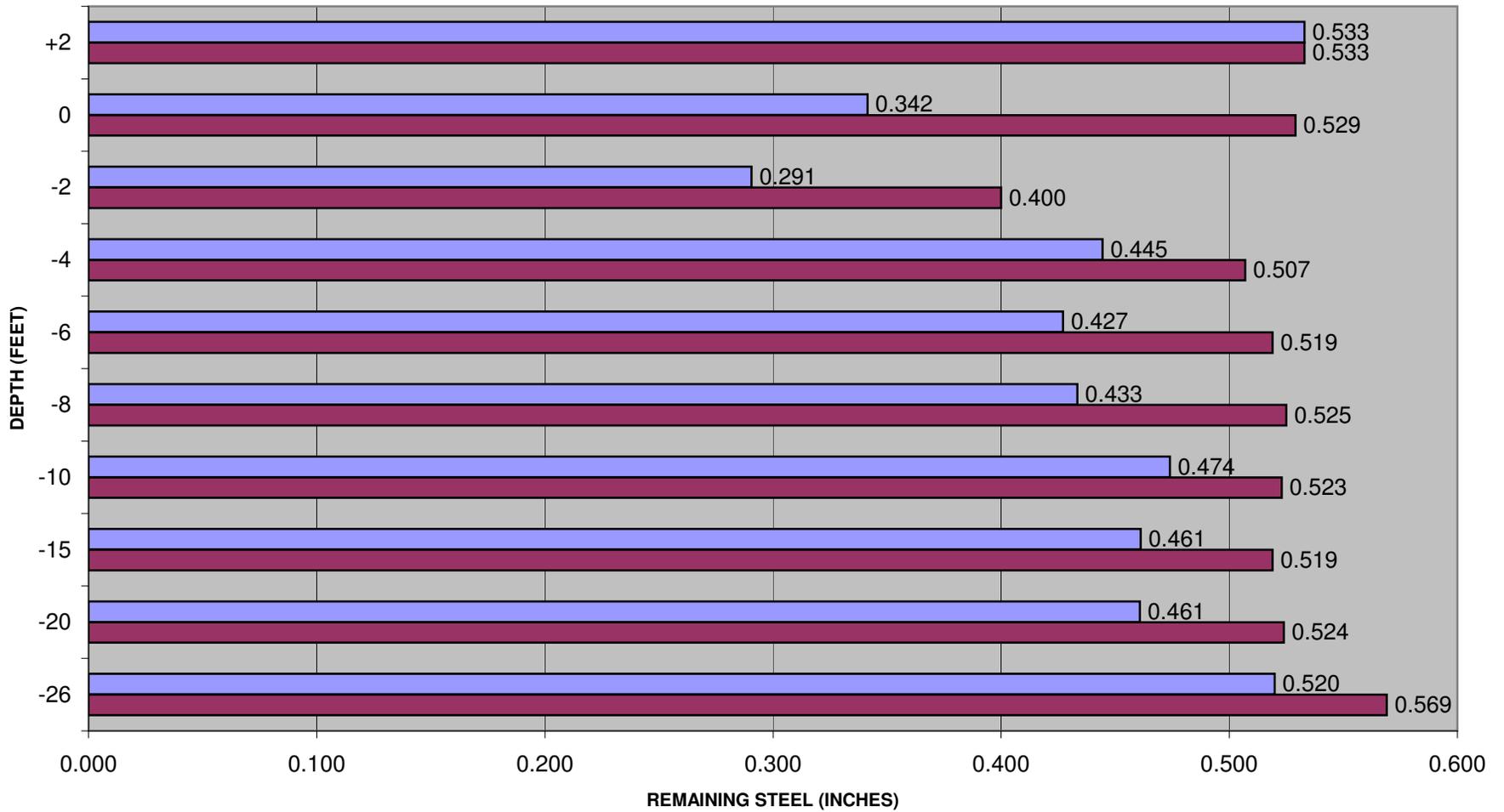


CENEX/ HARVEST STATES #3-REMAINING STEEL
SITE I.D. #16
(Measured Steel Thickness of 0.516 inches)

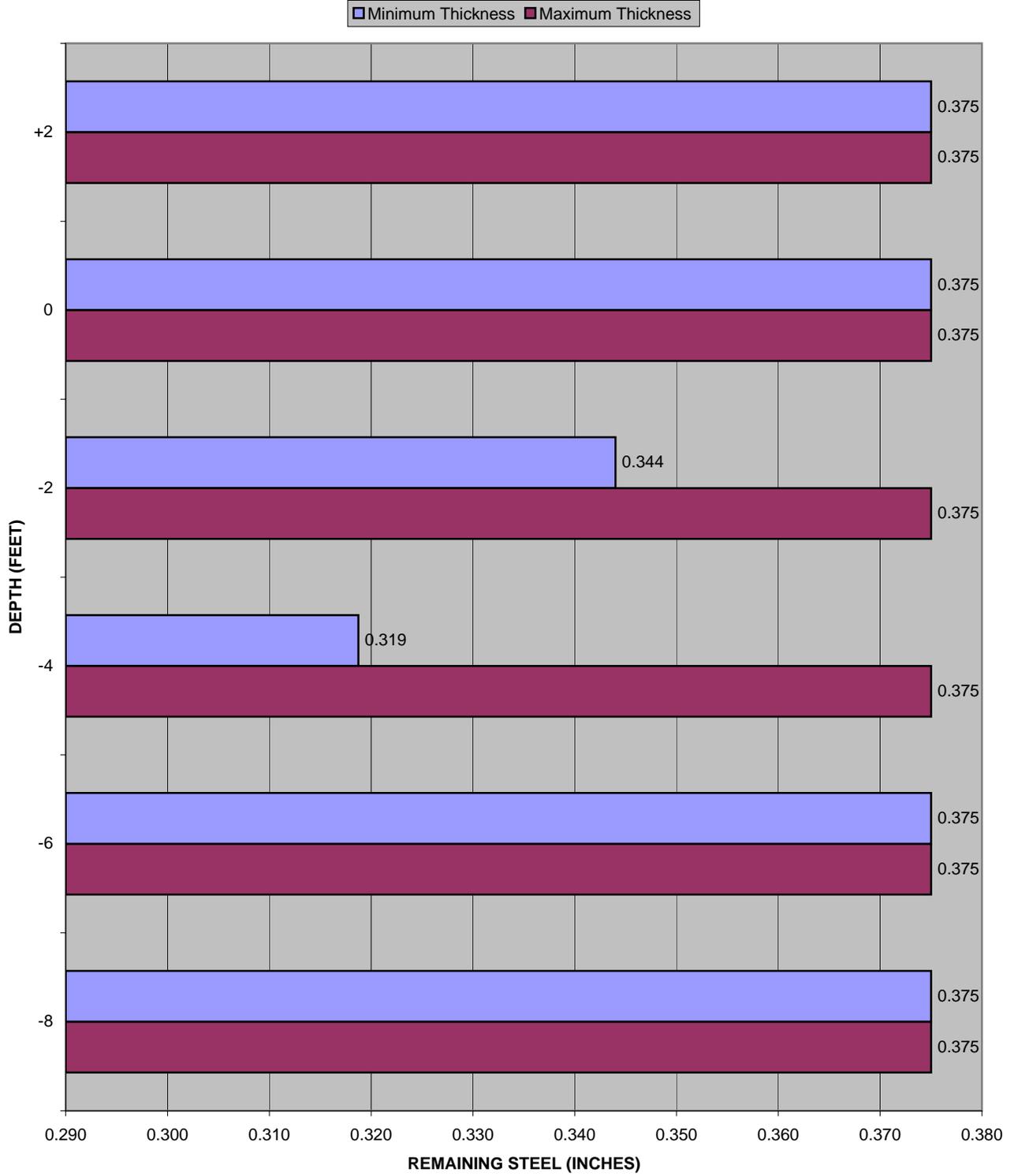


CUTLER MAGNER-REMAINING STEEL
SITE I.D. #17
(Measured Steel Thickness of 0.569)

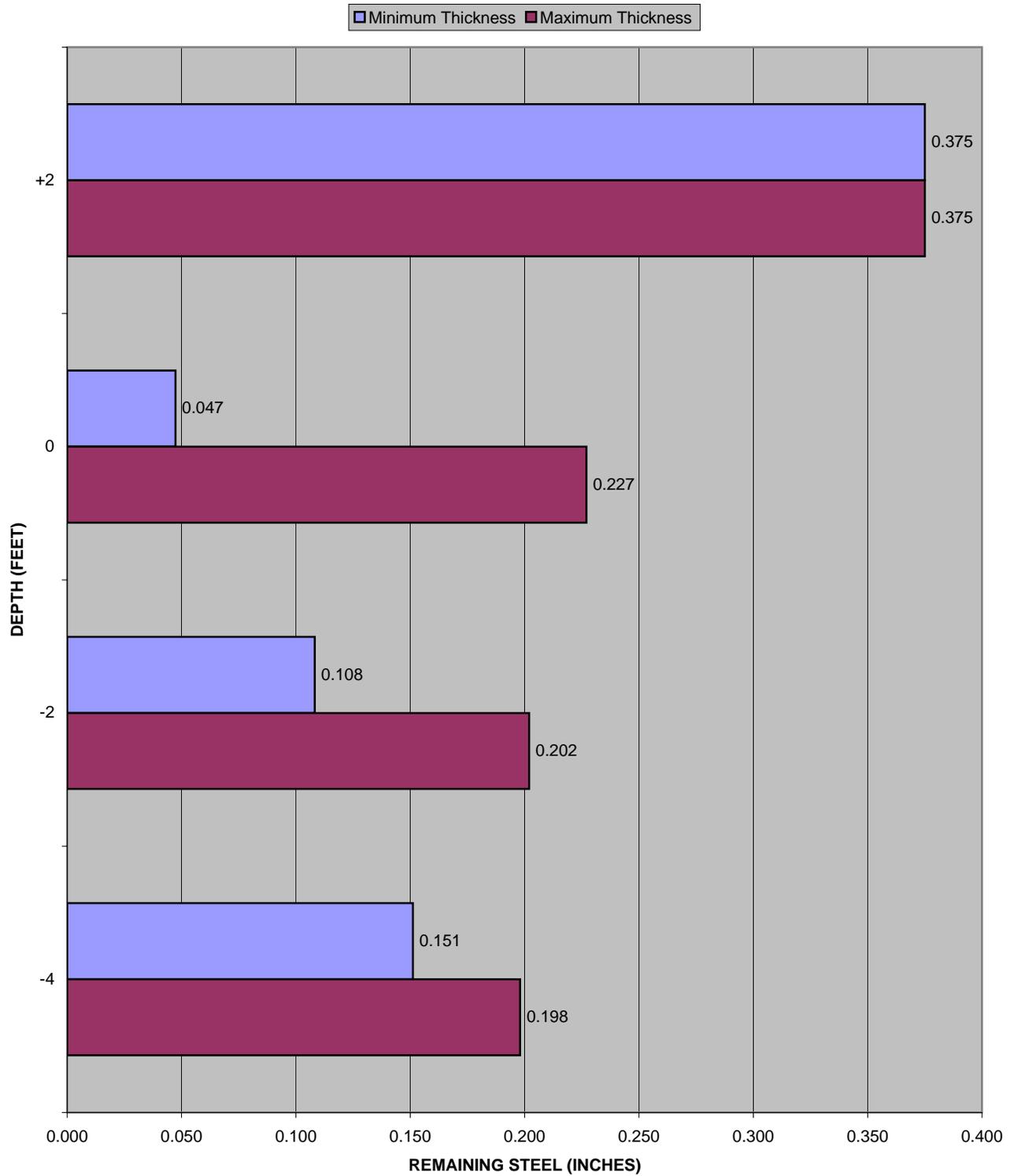
Minimum Thickness Maximum Thickness



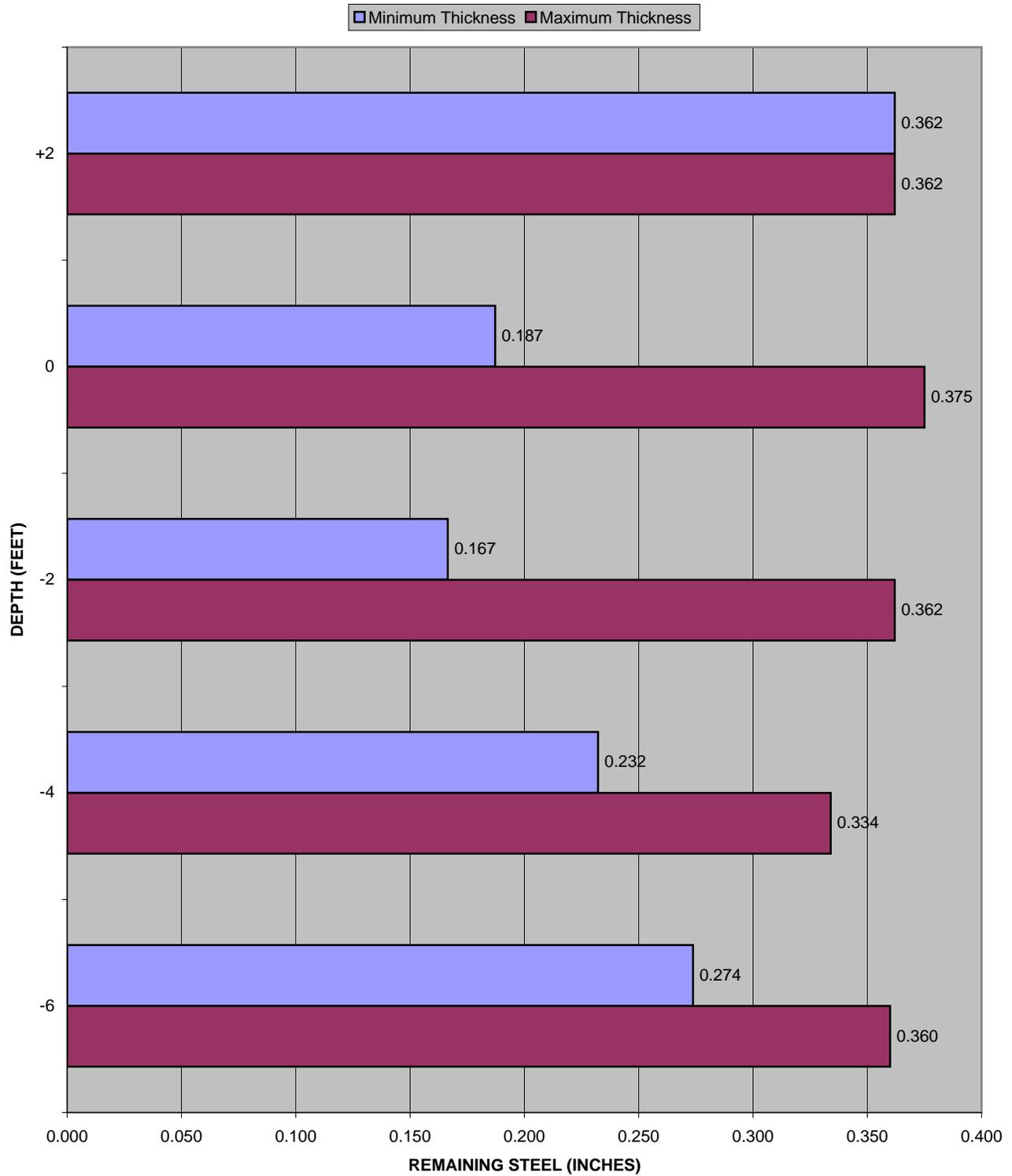
LAKEHEAD BOAT BASIN #1- REMAINING STEEL
SITE I.D. #18
(Measured Steel Thickness of 0.375 inches)



LAKEHEAD BOAT BASIN #2- REMAINING STEEL
SITE I.D. # 19
(Measured Steel Thickness of 0.375 inches)



COMMUNITY SAILING DOCK- REMAINING STEEL
SITE I.D. # 20
(Measured Steel Thickness of 0.362 inches)

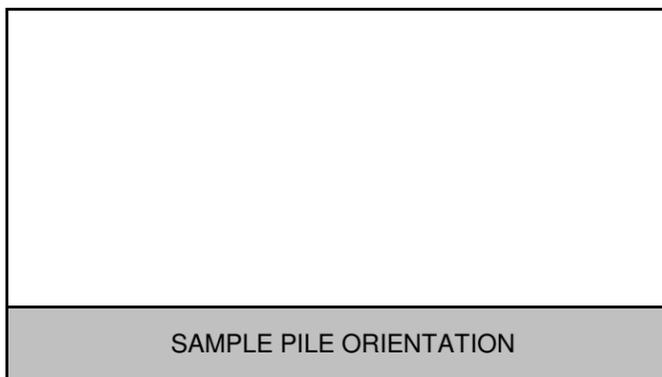


HARBOR STRUCTURES DATA



FACILITY William A Irvin Ship
 DOCK CONFIGURATION Ships Hull & Keel
 EXPOSURE DIRECTION Northeast

SITE I.D. NUMBER 21
 INSPECTION DATE 8/16/2006
 INSPECTION TIME 14:57
 WATER ELEVATION 601.66
 TEAM LEADER Chad Scott



SHEET PILE INFORMATION	TYPE	ORIG. THICK.	AGE
	Vessel Hull		Built 1938

STATION	Depth (IGLD +/-)	Marine Growth				Protective Coating				Corrosion			Steel Max. Remaining Thickness	Pit Penetration Readings					Pit Diameter Readings					Comments		
		Present	Type	Thickness	Coverage	Present	Type	Thickness	Coverage	Present	Type	Concentration (High Mod. Low)		Pit Penetration Readings					Pit Diameter Readings							
														1	2	3	4	AVG	1	2	3	4	AVG			
1	+2	x	Algae	<.25	20%	x	unk	unk																		
2	0	x	Algae	<.25	20%	x	unk	unk		x	Lrg.pits	High		0.250	0.188	0.188	0.219	0.211	0.375	0.500	0.375	0.625	0.469			
3	-2	x	Algae	<.25	20%	x	unk	unk		x	pits	High		0.188	0.156	0.188	0.219	0.188	0.625	0.625	0.625	0.625	0.625	High pitting on keel, low on hull		
4	-4	x	Algae	<.25	20%	x	unk	unk		x	pits	High Keel		0.156	0.156	0.125	0.125	0.141	1.000	0.750	0.750	0.625	0.781	High pitting on keel, low on hull		
5	-6	x	Algae	<.25	20%	x	unk	unk		x	pits	Mod		0.125	0.156	0.156	0.188	0.156	0.625	0.500	0.625	0.625	0.594	Hull coating has failed in some areas		
6	-8	x	Algae	<.25	20%	x	unk	unk		x	pits	Low		0.125	0.125	0.156	0.125	0.133	0.750	0.750	0.625	0.625	0.688	(See Video for Coatings Info)		
7	-10	x	Algae	<.25	20%	x	unk	unk		x	pits	Low		0.125	0.188	0.156	0.250	0.180	0.500	0.750	0.750	0.750	0.688			
8	-15																	0.000						0.000		
9	-20																	0.000							0.000	
10	ML																	0.000							0.000	



APPENDIX D

Water Quality Data Forms

Water Data



Facility	DSPA Berth 1
Site I.D. Number	1
Inspection Date	20-Jul-06
Inspection Time	9:24 AM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.79	8.7	0.142	3.1	67.2	320
3	-2	7.91	8.68	0.14	3.4	67.2	318
4	-4	7.94	8.68	0.14	3.4	67.2	315
5	-6	7.97	8.68	0.144	3.6	67.3	278
6	-8	7.98	8.68	0.144	3	67.3	275
7	-10	7.97	8.71	0.143	3.3	67.3	270
8	-15	7.94	8.74	0.14	3.5	66.4	258
9	-20	7.82	8.53	0.136	2.4	65.2	271
10	ML	7.62	8.9	0.122	23.1	60.6	220

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	DSPA Berth 4
Site I.D. Number	2
Inspection Date	20-Jul-06
Inspection Time	10:25

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.98	8.75	0.154	4.2	68.2	311
3	-2	7.98	8.65	0.155	4.1	68.1	310
4	-4	7.95	8.61	0.155	4.2	68	310
5	-6	7.94	8.51	0.154	4.1	67.8	310
6	-8	7.89	8.52	0.153	3.9	67.5	311
7	-10	7.89	8.49	0.153	3.9	67.6	312
8	-15	7.7	8.13	0.141	2.5	66.8	317
9	-20	7.8	8.88	0.139	4.6	64.2	317
10	ML	7.91	10.08	0.116	4.4	57.7	313

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	3.914954
Date ICR Measured	9/7/2006

Water Data



Facility	DSPA Berth 6
Site I.D. Number	3
Inspection Date	20-Jul-06
Inspection Time	11:50

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.86	8.43	0.159	5.5	68.3	319
3	-2	7.86	8.42	0.161	4.3	68.1	319
4	-4	7.82	8.51	0.162	5.2	67.8	319
5	-6	7.8	8.42	0.162	5	67.5	319
6	-8	7.79	8.37	0.162	5	67.5	317
7	-10	7.78	8.37	0.159	5.2	67	317
8	-15	7.77	8.34	0.158	5.6	66.8	318
9	-20	7.69	8.41	0.152	6.8	65.6	321
10	ML	7.66	8.41	0.137	14	63	297

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	CN Two Harbors
Site I.D. Number	4
Inspection Date	19-Jul-06
Inspection Time	2:30 PM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.84	10.34	0.103	1.3	60.3	266
3	-2	8.04	10.46	0.102	2.1	58.8	263
4	-4	8.04	10.49	0.103	2	57.9	269
5	-6	7.96	10.58	0.103	2.1	57.9	274
6	-8	7.96	10.63	0.103	3.2	57.8	274
7	-10	7.98	10.68	0.102	1.9	57.2	274
8	-15	8.06	10.79	0.102	2.4	56	270
9	-20	8.07	10.97	0.102	2.7	55.1	267
10	ML	8.04	11.68	0.102	5.6	49.4	257

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Minnesota Slip
Site I.D. Number	5
Inspection Date	8/2/2006
Inspection Time	11:35

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.71	6.3	0.185	19	74.5	454
3	-2	7.81	6.27	0.189	16.4	74.1	456
4	-4	7.8	6.34	0.19	17.2	73.7	456
5	-6	7.78	6.14	0.18	22.3	73.3	455
6	-8	7.74	5.76	0.169	30.1	72.5	454
7	-10	7.63	5.63	0.164	33.2	72.8	453
8	-15	7.64	5.69	0.155	30.4	71.5	453
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	DECC
Site I.D. Number	6
Inspection Date	8/2/2006
Inspection Time	8:05 AM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.93	7.32	0.151	10.9	73.2	448
3	-2	7.96	7.24	0.151	10.7	73.2	448
4	-4	7.96	7.07	0.151	9.6	73.2	450
5	-6	7.95	6.99	0.143	9.3	73	451
6	-8	7.99	7.14	0.137	9.9	72.7	451
7	-10	7.99	7.12	0.137	9.4	72.7	451
8	-15	8.02	7.4	0.126	9.7	71.9	454
9	-20	8.05	7.4	0.126	10.3	71.8	454
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Cargill Berth 1
Site I.D. Number	7
Inspection Date	8/2/2006
Inspection Time	12:50

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.97	7.08	0.145	9.4	73.9	
3	-2	8	7.07	0.144	9.5	73.8	
4	-4	8.04	7.16	0.145	9.8	73.8	
5	-6	8.04	7.18	0.145	9.8	73.8	
6	-8	8.06	7.21	0.145	9.9	73.8	
7	-10	8.03	7.06	0.143	8.9	73.6	
8	-15	7.95	7.06	0.121	10.2	71.8	
9	-20	7.86	7.07	0.121	9.5	71.7	
10	ML	7.96	7.64	0.111	9.5	70.5	

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Hallet Dock 5
Site I.D. Number	8
Inspection Date	8/1/2006
Inspection Time	1:45 PM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.79	6.62	0.192	9.8	77.2	462
3	-2	7.98	6.21	0.189	9.6	77	463
4	-4	7.95	6.12	0.187	9.8	76.9	462
5	-6	7.96	6.15	0.186	9.9	76.6	462
6	-8	7.93	6.02	0.186	9.2	76.6	462
7	-10	7.92	5.99	0.186	9	76.5	462
8	-15	7.92	5.96	0.184	10.1	76.4	462
9	-20	7.92	5.96	0.186	10.7	76.2	461
10	ML	7.89	5.86	0.208	15.8	75.2	422

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	6.357016
Date ICR Measured	9/7/2006

Water Data



Facility	Bong Bridge Cell
Site I.D. Number	9
Inspection Date	8/1/2006
Inspection Time	2:15 PM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	8.11	6.3	0.166	14.8	77.8	449
3	-2	8.1	6.18	0.166	16.4	77.8	449
4	-4	8.1	6.2	0.166	14.4	77.9	450
5	-6	8.1	6.24	0.166	15.2	77.9	450
6	-8	8.09	6.22	0.166	15.2	77.9	450
7	-10	8.08	6.22	0.165	14	77.9	450
8	-15	8.08	6.23	0.166	14.3	77.8	451
9	-20	8.09	6.24	0.166	14.3	77.9	451
10	ML	8.1	6.28	0.166	15.1	77.9	451

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Spirit Lake Marina
Site I.D. Number	11
Inspection Date	31-Jul-06
Inspection Time	2:34 PM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	8.2	6.8	0.175	9.1	84.8	442
3	-2	8.26	7.11	0.174	10.2	80.6	449
4	-4	8.22	7.05	0.174	10.1	78.8	454
5	-6	8.24	6.78	0.174	10.2	78.7	457
6	-8	8.25	6.68	0.174	10.6	78.7	459
7	-10	8.25	6.44	0.174	14.9	78.6	459
8	-15						
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Oliver Bridge
Site I.D. Number	12
Inspection Date	7/31/2006
Inspection Time	1:15 PM

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	8.14	6.62	0.193	14	79.3	498
3	-2	8.23	6.62	0.193	14.2	79.1	494
4	-4	8.24	6.62	0.193	14.5	79.2	493
5	-6	8.24	6.67	0.193	14.6	79.1	493
6	-8	8.25	6.81	0.193	14.4	79.1	493
7	-10	8.26	6.66	0.193	14.6	79.0	493
8	-15	8.24	6.67	0.193	14.8	79.0	494
9	-20	8.24	6.7	0.193	15.3	78.8	493
10	ML	8.26	6.64	0.193	16.1	78.8	491

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Corrosion Rate (mpy)	5.748697
Date ICR Measured	9/7/2006

Water Data



Facility	MERC
Site I.D. Number	13
Inspection Date	8/3/2006
Inspection Time	12:05

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen	Conductivity	Turbidity	Temperature	ORP
2	0	7.86	6.27	0.183	11.9	76.3	444
3	-2	7.91	6.29	0.182	12.4	76.3	442
4	-4	7.91	6.31	0.182	12.5	76.2	442
5	-6	7.91	6.33	0.183	12.5	76.2	443
6	-8	7.91	6.34	0.183	12.6	76	443
7	-10	7.91	6.35	0.184	12.3	76	444
8	-15	7.9	6.31	0.184	12.7	75.6	445
9	-20	7.88	6.33	0.178	12.8	75	447
10	ML	7.86	6.63	0.157	11.1	73.5	449

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	6.093998
Date ICR Measured	9/7/2006

Water Data



Facility	CHS East Dock
Site I.D. Number	14
Inspection Date	8/4/2006
Inspection Time	14:50

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.78	5.58	0.179	13	77.5	423
3	-2	7.76	5.58	0.178	13.5	77.5	425
4	-4	7.66	5.31	0.181	12.7	75.9	430
5	-6	7.66	5.28	0.179	13.3	75.2	431
6	-8	7.66	5.27	0.178	12.9	75	432
7	-10	7.59	4.44	0.173	14.2	74.4	438
8	-15	7.62	5	0.164	15.1	73.6	439
9	-20	7.58	4.74	0.162	20.8	73.4	440
10	ML	7.55	5.63	0.155	48.6	73	402

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	CHS West Dock (inner end)
Site I.D. Number	15
Inspection Date	8/4/2006
Inspection Time	15:30

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.89	6.05	0.182	17.9	78	426
3	-2	7.87	5.81	0.182	17	77.9	426
4	-4	7.85	5.84	0.183	16.7	77.6	426
5	-6	7.84	5.45	0.183	16.2	77.4	426
6	-8	7.75	5.22	0.19	17.3	75.4	430
7	-10	7.75	4.9	0.192	20.7	75.3	431
8	-15	7.74	4.63	0.186	28.6	74.1	432
9	-20	7.68	4.46	0.215	30.6	73.6	434
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	CHS (New Sheets)
Site I.D. Number	16
Inspection Date	8/4/2006
Inspection Time	15:50

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.9	5.87	0.182	19.2	78.3	444
3	-2	7.89	5.87	0.182	18.6	78	443
4	-4	7.88	5.84	0.182	18.4	77.9	442
5	-6	7.86	5.37	0.185	17.3	76	442
6	-8	7.76	4.97	0.19	19.3	75.4	444
7	-10	7.75	5.15	0.181	17.3	74.8	444
8	-15	7.71	4.95	0.191	19.4	73.9	446
9	-20	7.69	4.65	0.224	27.4	73.6	447
10	ML	7.71	5.09	0.258	23.1	73.4	448

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Cutler Magner
Site I.D. Number	17
Inspection Date	8/9/2006
Inspection Time	935

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	7.99	7.99	0.161	11.8	73.9	486
3	-2	8.01	7.55	0.161	10.4	73.9	484
4	-4	8.02	7.4	0.161	10.8	73.7	483
5	-6	8.02	7.09	0.161	11	73.3	483
6	-8	7.97	7.13	0.161	11.5	73	483
7	-10	7.95	6.81	0.16	10.7	72.9	483
8	-15	7.82	6.36	0.15	8.9	72.1	484
9	-20	7.82	6.61	0.146	9.8	71.7	484
10	ML	7.81	6.16	0.135	12.2	70.7	478

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Lakehead Boat Basin 1
Site I.D. Number	18
Inspection Date	8/4/2006
Inspection Time	13:50

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	8.03	7.83	0.134	8.7	72.4	459
3	-2	8.01	7.82	0.132	9.1	72.7	458
4	-4	7.99	7.9	0.124	11.2	71.5	456
5	-6	8.02	7.99	0.122	12.2	71.3	454
6	-8	8.09	7.96	0.122	12.6	71.2	445
7	-10						
8	-15						
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Lakehead B. Basin 2
Site I.D. Number	19
Inspection Date	8/4/2006
Inspection Time	2:15

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
1	2	8.08	7.72	0.135	14.7	73.5	453
2	0	7.91	7.76	0.134	15.0	73.4	457
3	-2	7.93	7.83	0.134	19.2	73.4	457
4	-4						
5	-6						
6	-8						
7	-10						
8	-15						
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	Community Sailing Dock
Site I.D. Number	20
Inspection Date	8/2/2006
Inspection Time	1520

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	8.13	7.5	0.145	17	77.4	468
3	-2	8.17	7.51	0.145	15.7	76.7	464
4	-4	8.11	7.26	0.146	16	76.4	463
5	-6						
6	-8						
7	-10						
8	-15						
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	

Water Data



Facility	John Sherwin
Site I.D. Number	21
Inspection Date	8/16/2006
Inspection Time	1640

Quanta Water Quality Data							
Station	Depth (IGLD +/-)	pH	Dissolved Oxygen Mg/L	Conductivity (mS/cm)	Turbidity (NTU)	Temperature (°F)	ORP (mV)
2	0	9.41	10.86	2.17	17	77	493
3	-2	9.31	10.5	0.217	17	76.4	498
4	-4	8.49	8.16	0.217	14.4	73	497
5	-6	8.28	7.71	0.218	14.4	71.6	503
6	-8	8.19	7.48	0.218	14.8	71.3	504
7	-10	8.06	7.05	0.218	15.6	70.9	506
8	-15	8.01	6.82	0.219	15.6	70.8	489
9	-20						
10	ML						

Bulk Water Sample Data @ -4 ft LWD				
Sample Taken			Sample Tested	
Date	Time		Date	Time
Chloride Ions				
Total Suspended Solids				
Hardness				
Total Iron				
Alkalinity				

Instantaneous Corrosion Information	
Instantaneous Corrosion Rate	
Date ICR Measured	



APPENDIX E

Linear Polarization Resistance Results & Report



BUSHMAN & Associates, Inc.

CORROSION CONSULTANTS

P.O. Box 425, Medina, OH 44258 • Phone 330/769-3694, Fax 330/769-2197

September 10, 2006

AMI Consulting Engineers
1 East 1st Street, Suite 403
Duluth, MN 55802

Attn: Mr. Chad W. Scott

Re: Duluth Harbor Corrosion Rate Testing

Dear Mr. Scott.

This letter report is intended to provide a summary of the test data and information obtained during our corrosion rate testing work performed on September 7, 2006 in Duluth Harbor. The methodology used is commonly referred to as Linear Polarization Resistance (LPR) Corrosion Rate Measurement which is defined in ASTM's Standard G59-97(2003), "Standard Test Method for Conducting Potentiodynamic Polarization Resistance Measurements".

The method used in this study follows the ASTM procedure using a Gamry Reference 600 Potentiostat, Galvanostat, and Zero Resistance Ammeter combined in a portable instrument package which is designed for both laboratory and field testing work. The unit requires a PC computer running under Windows 2000 or XP using Gamry's DC-105 Corrosion Measurement and Analysis software.

LPR is probably the most common test method used in assessing the corrosivity of an environment with respect to a metal. It is both relatively simple to perform, given the right computer driven test equipment, and provides reproducible results. At the end of each computer controlled scan, it automatically calculates the average corrosion rate over the surface area of the metal sample being testing in the water or soil being evaluated. Since underground and submerged metal corrosion is almost always of the pitting type, it is common practice to multiply this average rate by a factor of 5, 10 or 20 to determine the pitting or perforation rate that can be expected. B&A often uses a rate of 7.5 times the average rate as a reasonable approximation of the pitting rate.

LPR, as performed by B&A in this as well as most studies, involves the use of extremely small amounts of current (generally in the micro-ampere level) applied from a small metallic rod (commonly called the "counter electrode") to a prepared metal test specimen (commonly called the "working electrode") of the same metal alloy of that of the structure being evaluated when it is immersed in water or soil obtained from the environment in which the structure is or will be installed. The entire test is controlled by a microcomputer controlled DC power supply called a potentiostat. During the entire LPR scan, the energy level (or potential) of the metal specimen is measured in millivolts by a reference electrode. The applied current is controlled to vary the potential of the metal specimen in a series of steps from a value of 20 millivolt less than the free corrosion potential to a value 20 millivolt more positive than the free corrosion potential.

The test scan parameter from **Scan #4 at Midwest Energy Dock** using the insitu probe with Serial. No. 06-08-1008 installed approximately 1½ weeks ago were as follows;

Initial E (V): -0.02 vs. Eoc
Final E (V): 0.02 vs. Eoc
Test Setup: Linear Polarization Resistance
Date: 9/7/2006
Time: 13:37:18
Scan Rate (mV/s): 0.2
Sample Period (s): 2
Sample Area (cm²): 5
Steel Density (gm/cm³): 7.87
Steel Equiv. Wt: 27.92
Conditioning: Off
Init. Delay: On
Time for stabilization before starting scan (s): 100
Stab.(mV/s): 0.1
Open Circuit (V): 0.006856

When this data is plotted on a semi-log graph, a linear relationship between the change in potential versus the applied test current is observed.



Figure 1 - B&A Computer Running Gamry LPR Software in Duluth Harbor

Once the experiment is complete, the data generated is sent to the Gamry Analysis Package which permits calculation of the average corrosion rate based on the slope and axis intercept point of the line developed during the LPR scan. The program then displays the analysis determinations as follows:

EXPERIMENTAL DETERMINATIONS (from Scan #4 at Midwest Energy Dock)

Beta An.(V/Dec): 0.12

Beta Cat.(V/Dec): 0.12

Icorr (A): 6.599473E-05

Ecorr (V): 5.72136E-03

Corrosion Rate (mpy): 6.031089

Since pitting corrosion is visibly occurring; B&A calculates a real corrosion penetration rate of 45.2 mils per year (mpy) or penetration of a 1/2" plate in 11 years.



Figure 2 - LPR Test Probe Junction Box



Figure 3 - LPR Probe after 1 week exposure



Figure 4 - LPR Test Probe Tips after 2 weeks exposure



Figure 5 - Gamry 600 LPR Instrument Supported by Ladder



Fig 6 – Test Setup with Computer on Boat



Fig 7 – AMI Inspection Boat used for all tests



Fig 8 – All tests were controlled from this location



Fig 9 – AMI performing water chemistry tests



Fig 10 – AMI Hach Water Chemistry Probe



Fig 11 – Hach Water Chemistry Display

LPR Scans were measured at the 7 sites with 3 scans per site. Results are summarized in the following table:

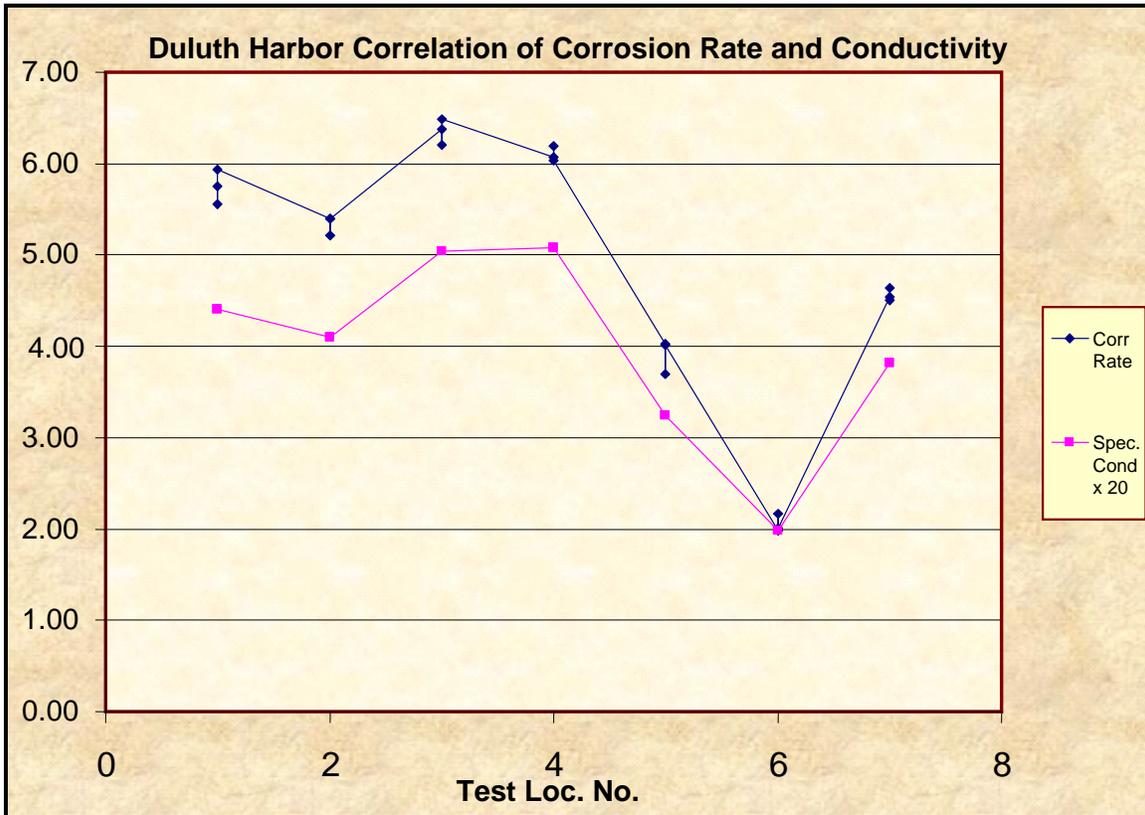
Table No. 1 – Corrosion Rate Test Results – Duluth Harbor

Location Description	Test Locate No.	Scan No.	LPR Probe Ser. No.	Corrosion Rate (mpy)
Oliver Bridge	1	B	Ser. No. 06-98-1005	5.750072
Oliver Bridge	1	C	Ser. No. 06-98-1005	5.554085
Oliver Bridge	1		Ser. No. 06-98-1005	5.941934
Hallett 7 Dock	2	A	Ser. No. 06-08-1003	5.400351
Hallett 7 Dock	2	B	Ser. No. 06-08-1003	5.207576
Hallett 7 Dock	2		Ser. No. 06-08-1003	5.403211
Hallett 5 Dock	3	A	Ser. No. 06-08-1007	6.367826
Hallett 5 Dock	3	B	Ser. No. 06-08-1007	6.209100
Hallett 5 Dock	3		Ser. No. 06-08-1007	6.494123
Midwest Energy Dock	4	A	Ser. No. 06-08-1008	6.065133
Midwest Energy Dock	4	B	Ser. No. 06-08-1008	6.185771
Midwest Energy Dock	4		Ser. No. 06-08-1008	6.031089
DSPA Berth 4	5	A	Ser. No. 06-08-1004	4.030746
DSPA Berth 4	5	B	Ser. No. 06-08-1004	3.699939
DSPA Berth 4	5		Ser. No. 06-08-1004	4.014178
US Army COE Duluth Entry	6	A	Ser. No. 06-08-1006	1.977549
US Army COE Duluth Entry	6	B	Ser. No. 06-08-1006	2.165742
US Army COE Duluth Entry	6		Ser. No. 06-08-1006	2.012401
Superior Cutler Magner	7	A	Ser. No. 06-08-1009	4.541889
Superior Cutler Magner	7	B	Ser. No. 06-08-1009	4.641087
Superior Cutler Magner	7		Ser. No. 06-08-1009	4.496408

The above rates are considerably higher than normally measured by B&A in potable waters. More typically, we would have expected values in the 0.5 to 1.5 mil/year corrosion rate. We then decided to analyze the probable correlation between the measured water conductivity and the measured corrosion rates. To show these on the same graph, the specific conductivity values were all multiplied by 20 to produce numeric values that would be in the same range as those provided by the Corrosion Rate Values. There is an obvious close relationship between the values as would be expected. None-the-less, the corrosion rates are so high that they can only be explained by some other over-riding factor accelerating the rate such as micro-biologically influenced corrosion (MIC).

We have attached copies of all LPR scans, thumbnail prints of all photos taken (including CDs with high resolution copies thereof) as well as a tabulation of the above with the additional water chemistry data measured by AMI Consulting Engineers.

Graph 1 – Correlation between Corrosion Rate and Conductivity



Recommendations:

- It is imperative that another set of readings be made in approximately 1 month to see if there is any measurable decline in these corrosion rates.
- Test for MIC using several available techniques to determine if this is a principal impactor on the unusually high corrosion rates being experience in the Duluth Harbor.
- Test for Stray DC Currents including those that might be emanating from the nearby HVDC system and from DC powered ship loading conveyors.
- Develop and implement a remediation plan for saving that piling which has not already suffered excessive corrosion. This plan needs to be “trialed” as soon as possible.

We sincerely appreciate having the opportunity of working with you on this project and the support and assistance provided by you and your staff at every step. If you have any questions or need further information from me, please call or write.

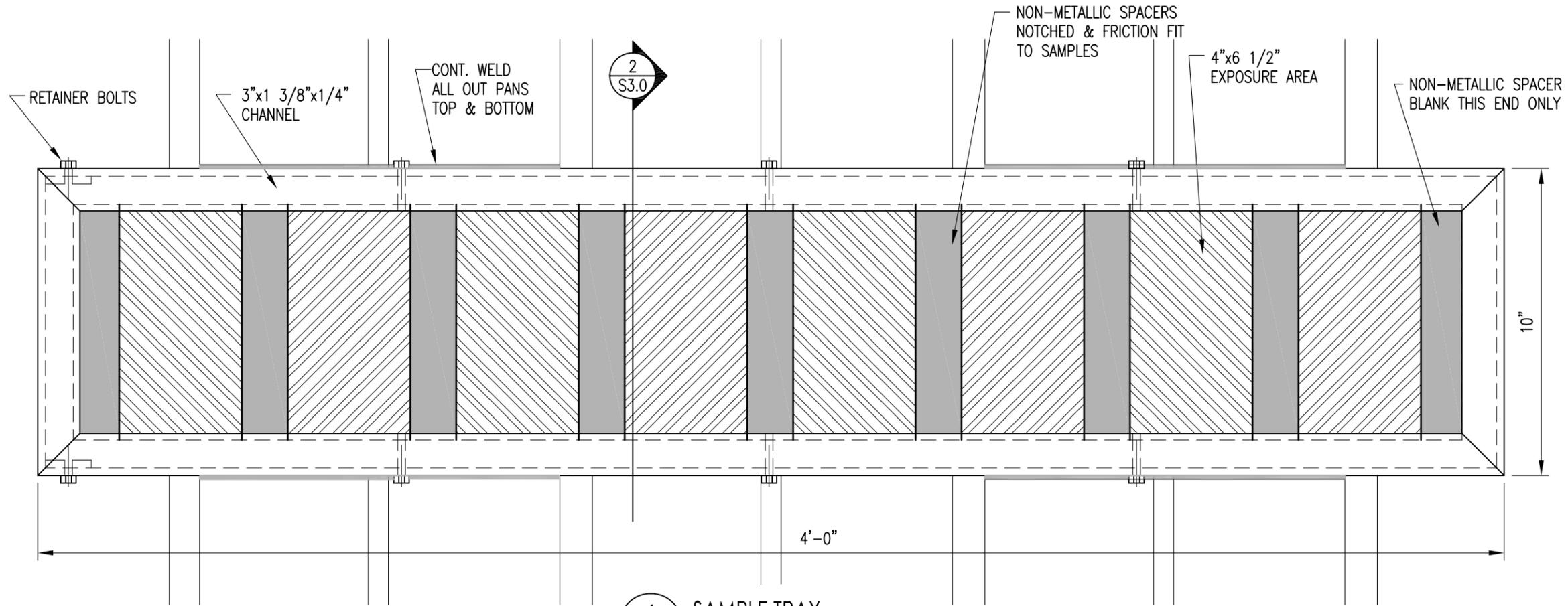
Sincerely,
Bushman & Associates, Inc.

James B. Bushman, P.E., C.P.S., S.C.T.
President and Principal Corrosion Engineer

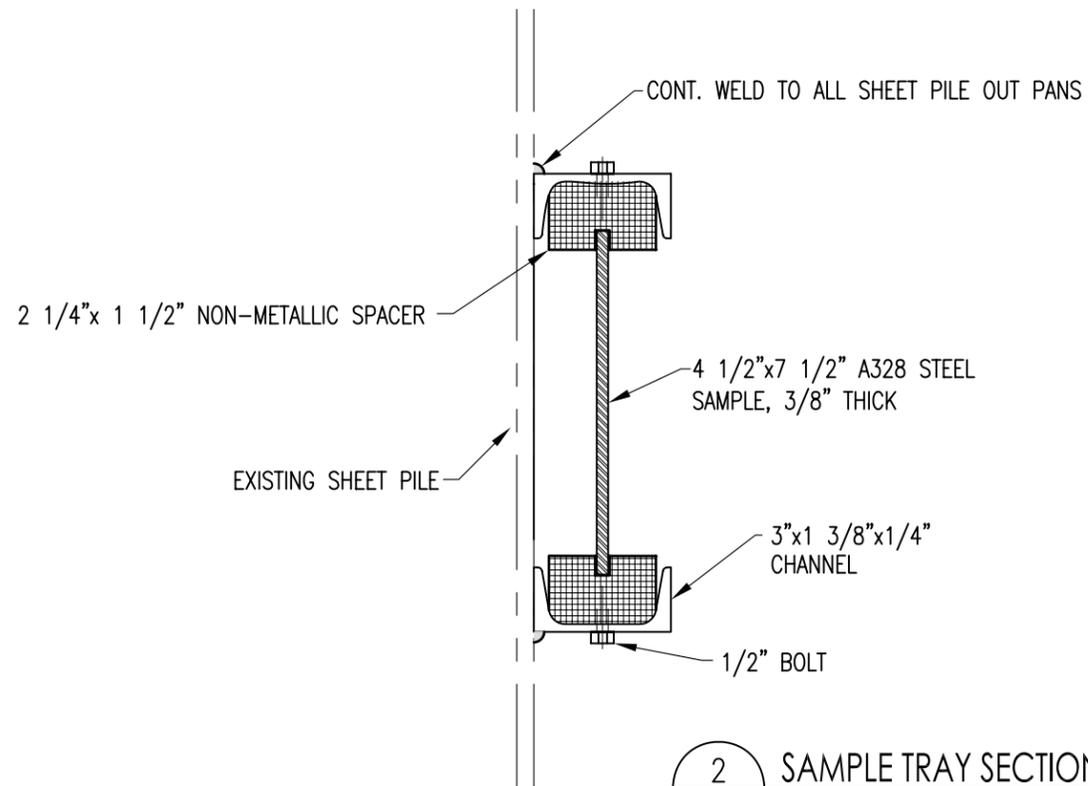


APPENDIX F

Sample Tray Plans and Data



1 SAMPLE TRAY
3" = 1'-0"



2 SAMPLE TRAY SECTION
3" = 1'-0"

DATE:	REV:	DESCRIPTION	BY:

USACE HARBOR CORROSION INVESTIGATION	DULUTH, MINNESOTA
STEEL COUPON SAMPLE TRAY #2	

JOB No: 061036
DATE: 10/20/06
DRAWN BY: SAJ
DESIGNED BY: CWS

SHEET:
S1.0



CORROSION SAMPLE TRAY INFORMATION				
Sample Tray Location	Dimensions (cm)		Weight	Installation
Steel Plate I.D.	Length	Width	(grams)	Date
DPSA BERTH 4				
B4- 1	19.3	11.6	1878.2	10/17/2006
B4- 2	19.4	11.7	1896.8	10/17/2006
B4- 3	19.4	11.4	1869.1	10/17/2006
B4- 4	19.3	11.6	1894.9	10/17/2006
B4- 5	19.3	11.7	1866.5	10/17/2006
B4- 6	19.3	11.6	1886.1	10/17/2006
B4- 7	19.4	11.7	1891.5	10/17/2006
B4- 8	19.2	11.5	1855.9	10/17/2006
AVERAGES	19.325	11.6	1879.88	
HALLETT DOCK 5				
H5- 1	19.3	11.7	1861	10/17/2006
H5- 2	19.4	11.5	1787.5	10/17/2006
H5- 3	19.3	11.5	1870.1	10/17/2006
H5- 4	19.7	11.7	1872.9	10/17/2006
H5- 5	19.4	11.8	1881.6	10/17/2006
H5- 6	19.3	11.8	1893.1	10/17/2006
H5- 7	19.5	11.6	1870.2	10/17/2006
H5- 8	19.4	11.6	1875.3	10/17/2006
AVERAGES	19.41	11.65	1863.96	
HALLETT DOCK 7				
H7- 1	19.5	11.5	1871.4	10/3/2006
H7- 2	19.4	11.6	1884.2	10/3/2006
H7- 3	19.3	11.7	1864.7	10/3/2006
H7- 4	19.4	11.6	1860.6	10/3/2006
H7- 5	19.4	11.8	1900.7	10/3/2006
H7- 6	19.5	11.6	1788.6	10/3/2006
H7- 7	19.4	11.7	1854	10/3/2006
H7- 8	19.2	11.5	1956.2	10/3/2006
AVERAGES	19.39	11.63	1872.55	
OLIVER BRIDGE				
OB- 1	19.4	11.6	1866.7	10/4/2006
OB- 2	19.4	11.6	1813.5	10/4/2006
OB- 3	19.3	11.5	1854.1	10/4/2006
OB- 4	19.2	11.7	1885.3	10/4/2006
OB- 5	19.3	11.5	1899.9	10/4/2006
OB- 6	19.2	11.4	1817.6	10/4/2006
OB- 7	19.3	11.5	1895	10/4/2006
OB- 8	19.3	11.4	1866.7	10/4/2006
AVERAGES	19.30	11.53	1862.35	



Sample Tray Location Steel Plate I.D.	Dimensions (cm)		Weight (grams)	Installation Date
	Length	Width		
MIDWEST ENERGY				
MW- 1	19.3	11.5	1860.8	10/17/2006
MW- 2	19.3	11.6	1871.5	10/17/2006
MW- 3	19.3	11.5	1883.8	10/17/2006
MW- 4	19.3	11.5	1835.7	10/17/2006
MW- 5	19.2	11.5	1864	10/17/2006
MW- 6	19.3	11.7	1916.3	10/17/2006
MW- 7	19.4	11.7	1908.8	10/17/2006
MW- 8	19.2	11.6	1892.6	10/17/2006
AVERAGES	19.29	11.58	1879.19	
CUTLER MAGNER				
CM- 1	19.3	11.5	1862.3	10/3/2006
CM- 2	19.2	11.7	1890.8	10/3/2006
CM- 3	19.4	11.6	1884.9	10/3/2006
CM- 4	19.3	11.6	1903.7	10/3/2006
CM- 5	19.2	11.7	1964.3	10/3/2006
CM- 6	19.4	11.6	1901.3	10/3/2006
CM- 7	19.3	11.6	1890.6	10/3/2006
CM- 8	19.3	11.5	1866.1	10/3/2006
AVERAGES	19.30	11.60	1895.50	

Balance used: NBS Serial #F54470 calibrated-4/19/06